

United States Naval Postgraduate School



THE SIS

SPECTRAL RADIANCE MEASUREMENTS IN MONTEREY BAY

by

Raymond Theodore Micheline

Thesis Advisor:

Stevens P. Tucker

September 1971

Thesis
M57534

Approved for public release; distribution unlimited.

United States Naval Postgraduate School



THE SIS

SPECTRAL RADIANCE MEASUREMENTS IN MONTEREY BAY

by

Raymond Theodore Michelini

Thesis Advisor:

Stevens P. Tucker

September 1971

Approved for public release; distribution unlimited.

TECHNICAL
NAVY POSTGRADUATE SCHOOL
MAYFIELD, CALIF. 93240

Spectral Radiance Measurements in Monterey Bay

by

Raymond Theodore Michelini
Lieutenant, United States Navy
B.S., United States Naval Academy, 1964

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN OCEANOGRAPHY

from the
NAVAL POSTGRADUATE SCHOOL
September 1971

ABSTRACT

An underwater spectral radiance meter having a rotating spectral wedge filter and capable of operating to depths of 300 meters was designed and constructed. It was used to obtain measurements of spectral radiance to a depth of 60 meters at two stations in southern Monterey Bay, California, on an overcast day during July 1971. Variations of the spectral radiance distribution with depth were plotted for vertical angles of 0, 45, 90, 135 and 166 degrees at an azimuth angle of zero degrees with respect to the sun.

The results of the measurements are reasonable in all cases and indicate that the spectral wedge filter provides a practical means of determining spectral radiance distributions.

TABLE OF CONTENTS

I.	INTRODUCTION	8
A.	PURPOSE	8
B.	PREVIOUS INVESTIGATIONS	8
II.	EQUIPMENT	12
A.	NPS SPECTRAL RADIANCE METER	12
1.	Photometer Unit	12
2.	Motor Housing Unit	23
3.	Junction Box	23
4.	Battery Supply	24
B.	CALIBRATION	24
1.	Azimuth and Vertical Angles	24
2.	Spectral Wedge Filter	24
3.	Acceptance Angle	29
4.	Photometer	29
III.	DATA COLLECTION	34
A.	STATION LOCATIONS	34
B.	OPERATIONAL PROCEDURES	34
IV.	DATA ANALYSIS	37
V.	CONCLUSIONS	41
APPENDIX A	Figures of Spectral Radiance Distribution with Depth at $\phi = 0^\circ$ and $\theta = 0, 45, 90, 135,$ and 166° for Stations 1 and 2	42

APPENDIX B	Spectral Radiance Calibration Nomograms for 25 nm Wavelength Bands from 400-725 nm -----	52
APPENDIX C	Station Data: Location, Date, Time, Depth, Weather, Altitude of the Sun, Azimuth of the Sun, Radiance Measurements -----	65
BIBLIOGRAPHY	-----	77
INITIAL DISTRIBUTION LIST	-----	80
FORM DD 1473	-----	85

LIST OF FIGURES

Figure

1.	Location of Stations in Monterey Bay -----	9
2.	Spectral Radiance Meter -----	13
3.	Radiance Meter Before Submergence -----	14
4.	General Arrangement of Radiance Meter -----	15
5.	General Arrangement of Photometer Unit -----	17
6.	Block Electrical Diagram of Underwater Unit -----	18
7.	Circuit Diagram of Shipboard Recording System -----	18
8.	Spectral Wedge Filter Characteristics -----	20
9.	Photometer Circuitry -----	21
10.	Overall Sensitivity Versus Overall Voltage -----	22
11.	Photomultiplier Tube Spectral Response -----	22
12.	Vertical Angle Calibration Curve in Downward Direction --	25
13.	Vertical Angle Calibration Curve in Upward Direction ----	26
14.	Azimuth Angle Calibration Curve -----	27
15.	Spectral Wedge Filter Rotation Calibration Curve -----	28
16.	Acceptance Angle Calibration Arrangement -----	30
17.	Acceptance Angle Calibration Curve -----	31
18.	System Calibration Arrangement -----	32
19.	Calibration Curve for Standard Lamp -----	33
20.	Uncorrected Spectral Radiance Variation with Depth at $\phi = 0^\circ$ and $\theta = 0, 45, 90, 135, \text{ and } 166^\circ$ -----	35
21.	Sample of Spectral Radiance Output -----	38

22-31.	Spectral Radiance Distribution with Depth at $\phi = 0^\circ$; $\theta = 0, 45, 90, 135$, and 166° for Stations 1 and 2	----- 42
32-44.	Spectral Radiance Calibration Nomograms for 25 nm Wavelength Bands from 400-725 nm	----- 52

ACKNOWLEDGEMENTS

The author gratefully acknowledges the support of all those people who helped in the preparation of this thesis. I am particularly indebted to my advisor, Stevens P. Tucker, for his continual support, cooperation, and technical guidance and to those personnel of the Naval Postgraduate School Machine Shop, particularly Mr. Peter Wisler, Mr. Jerry D. Smith, and MRCM Robert L. Wolfgram, USN, and to Mr. Dana Mayberry, our Oceanographic Electronic Technician, for their participation in the construction of the spectral radiance meter. This work was supported in part by Naval Air Systems Command.

I also wish to thank Professor Jerry A. Calt and the crew of the Naval Postgraduate School Hydrographic Boat for their assistance. Lastly, sincere thanks to my wife, Susanne, for her typing assistance, endless encouragement, and the positive manner in which she accepted my neglect during this effort.

I. INTRODUCTION

A. PURPOSE

With the increasing application of optical properties in the fields of water mass characterization, marine optical systems and biological studies there exists a strong need for more measurements of these properties and, in particular, measurements of underwater radiance with depth.¹

The purpose of my investigation was to measure the spectral radiance distribution of submarine daylight as a function of depth in Monterey Bay, California. To acquire these measurements a radiance meter using a rotating spectral wedge filter capable of continuous rotation in the vertical and horizontal planes was constructed between January and June 1971 at the Naval Postgraduate School. Measurements of spectral distribution of submarine daylight with depth were then made to a depth of 60 meters at two stations in Monterey Bay during July 1971 (Figure 1).

B. PREVIOUS INVESTIGATIONS

Historically, initial studies of radiant light intensity in the sea began during the early 1900's when scientists were successful in measuring spectral radiance with photographic techniques. Until about 1940

¹Radiant intensity (of a source in a given direction) is defined as the radiant flux emitted by a source, or by an element of a source, in an infinitesimal cone containing the given direction divided by the solid angle of that cone. The unit of measurement is expressed in watts per steradian. Radiance is the radiant flux per unit solid angle per unit projected area of a surface. Its units are watts per square meter per steradian.

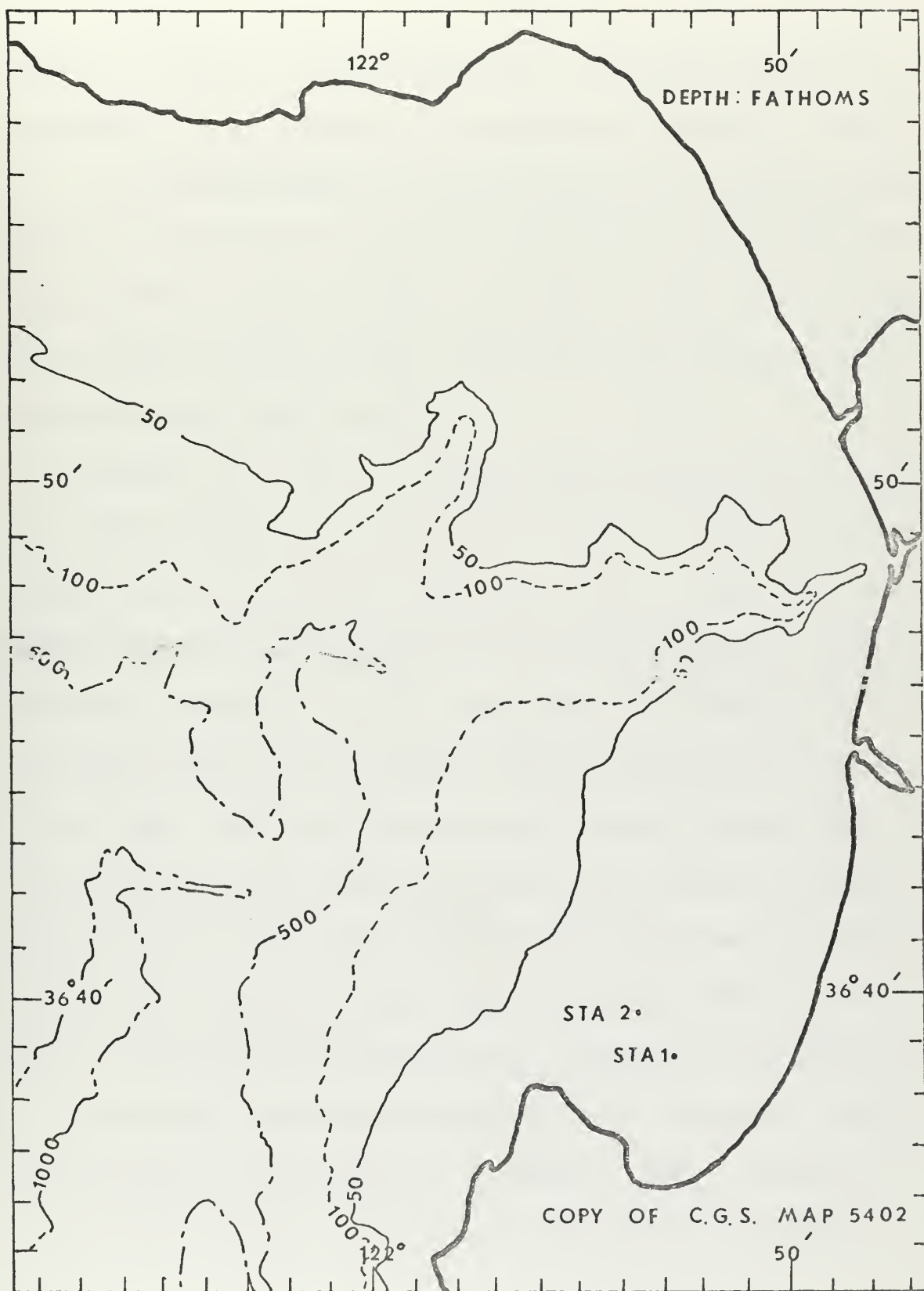


FIGURE 1. LOCATION OF STATIONS IN MONTEREY BAY

such recording systems were used to measure the variation of spectral radiance of submarine daylight with depth. Although the photographic techniques had many limitations the results were qualitatively useful.

With the development of sensitive photoelectric detectors and improvements in spectrographic instruments, the way was paved for much of the pioneer work in the field by Darby, Le Grand, Le Noble, Duntley, Jerlov, Tyler, Ivanoff, and many others. Since then, research progress has paralleled instrumental techniques.

Sasaki, et al., [1955a] initiated studies utilizing the photomultiplier tube in making radiance measurements from the underwater observation chamber KUROSHIO in Hakodate Bay, Japan. Using three Wratten gelatin filters he was able to determine the angular distribution pattern of light as a function of particular wavelengths. Employing the same photometer, Sasaki, et al., [1955b] examined natural light in the red, yellow, green, blue, and violet wavelength regions in waters of the Kuroshio Current, which enabled him to make some extinction coefficient determinations for the oceanic region. Similar studies were also being carried out by Duntley and Tyler at Lake Pend Oreille, Idaho [Duntley 1963]. The results of the latter studies supported the asymptotic radiance distribution hypothesis of the light field from the surface to great depths which was speculated by L. V. Whitney [1941]. Theoretical proof of the existence of this distribution was given by Preisendorfer [1959] .

With the advent of the second generation of radiance meters, interesting studies were subsequently made by Sasaki, Tyler, Jerlov, and many others throughout the world. A cumulative analysis of all their results clearly indicates that radiance becomes more symmetrical about the vertical and horizontal axes with depth; that a strong radiance maximum exists in the apparent direction of the sun; that radiance approaches an asymptotic distribution; that the variation of sea surface, sky and turbidity of the water have a large effect on the radiance distribution; and that the light "window" in the sea is in the 480 nanometer wavelength region.

More recently, extensive studies by Tyler and Smith [1970] of spectral irradiance underwater were made during 1968 with the Scripps Spectroradiometer at six locations in the Northern Hemisphere and yielded quantitative information related to the optical attenuation properties and the spectral distribution of underwater light.

Locally, the only previous study of underwater illumination was made by Bassett and Furminger in Monterey Bay in 1964 [Bassett and Furminger 1965]. They found the diffuse attenuation coefficient (vertical extinction coefficient) to be about $.090 \text{ m}^{-1}$ at 536 nm for their Monterey Bay stations in January 1965.

II. EQUIPMENT

A. NPS SPECTRAL RADIANCE METER

A spectral radiance meter capable of continuously measuring the spectral intensity of submarine daylight over 4π steradians to a depth of 750 feet was designed by the author and Stevens P. Tucker. Since the results of Sasaki's shallow water studies [Sasaki, et al. 1955b] have shown that the direction of the maximum value of the angular distribution of submarine daylight in the horizontal plane is always identified with the solar bearing, it was decided not to include a direction sensor to determine the orientation of the meter when submerged.

The radiance meter (Figures 2 and 3) consists of three major units plus an underwater battery supply: the photometer unit, the motor housing, and the junction box. The general arrangement of the components within the meter is shown in Figure 4. A block electrical diagram of the entire underwater unit and the shipboard recording system are shown in Figures 6 and 7.

During operation the entire underwater unit is suspended from a 3/16-inch O.D., 4-conductor, armored electrical cable.

1. Photometer Unit

The photometer is housed in a 12-inch long aluminum tube having a 3/4-inch wall thickness and an inside diameter of 6 inches. The unit is attached by clamps to the horizontal shaft of the motor housing,

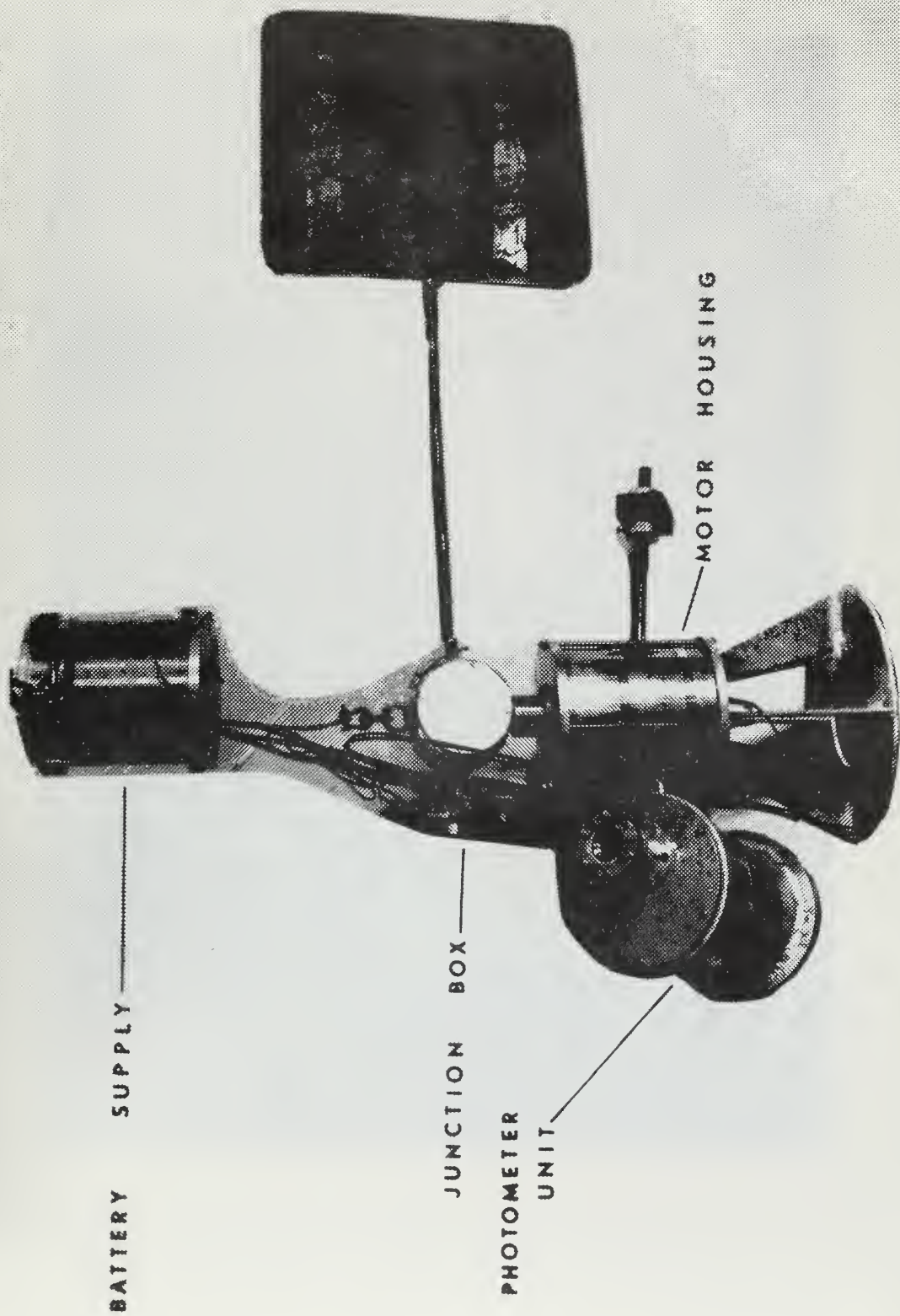


FIGURE 2. SPECTRAL RADIANCE METER

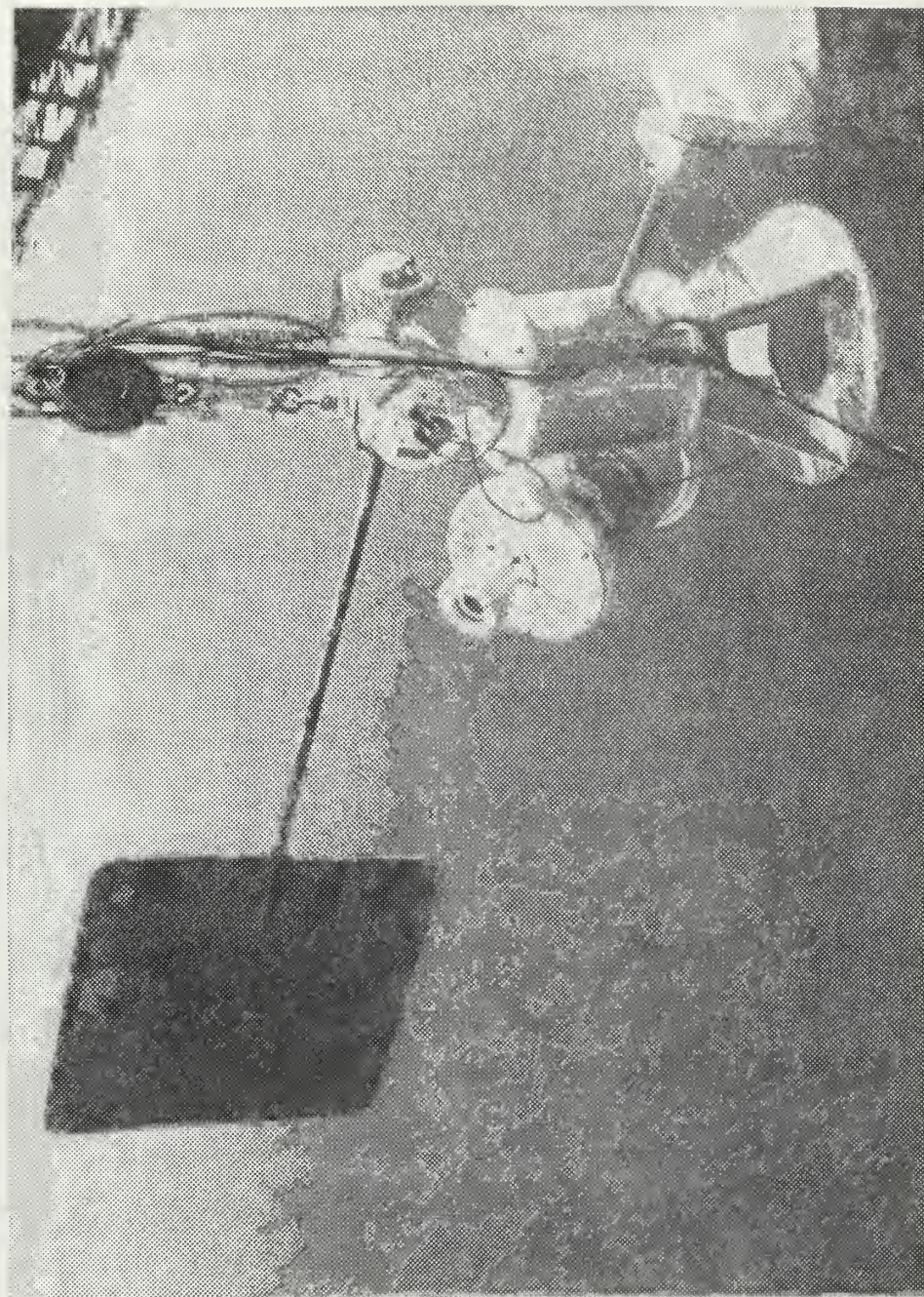


FIGURE 3. RADIANCE METER BEFORE SUBMERGENCE

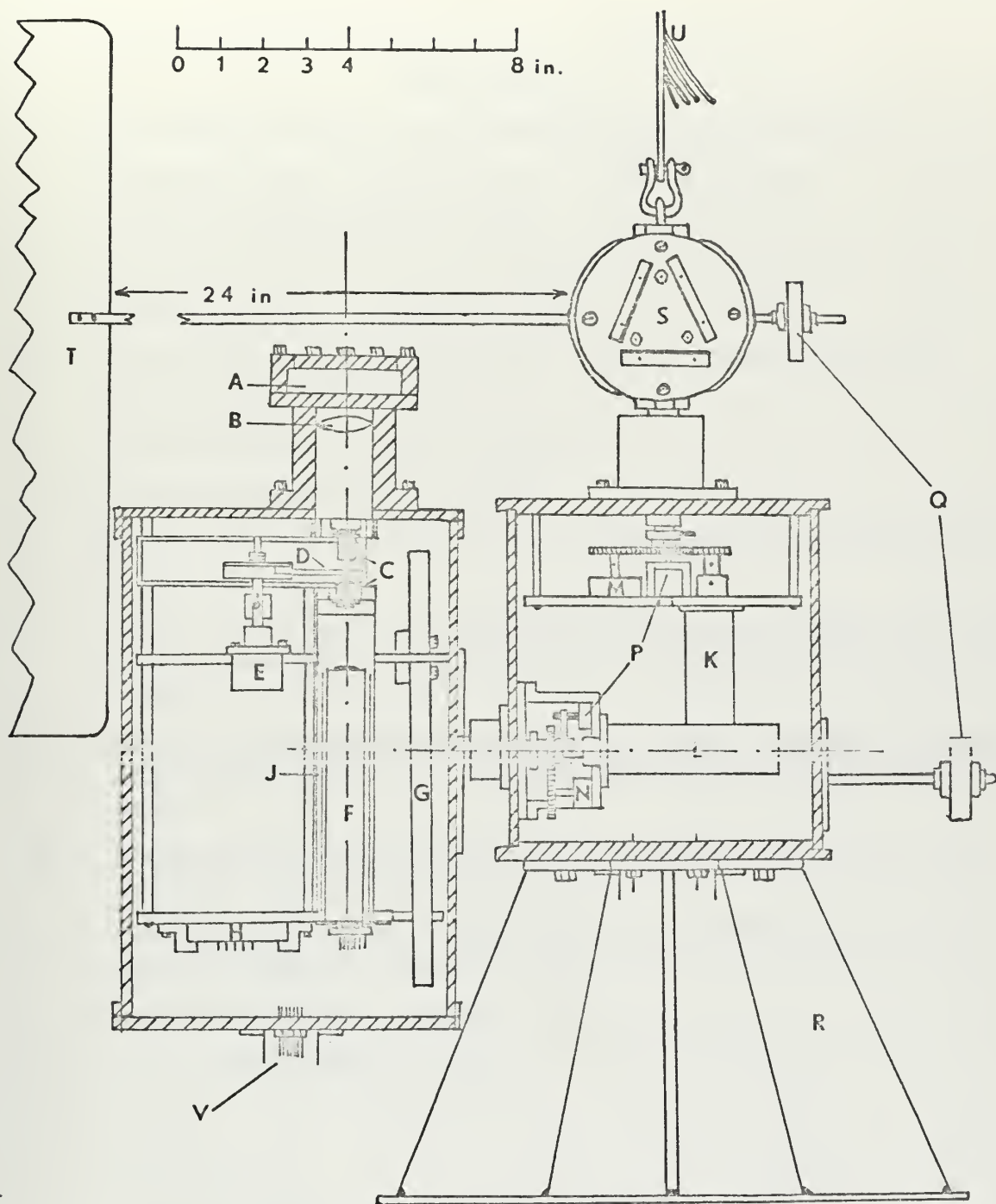


FIGURE 4. GENERAL ARRANGEMENT OF RADIANCE METER
(SEE PAGE 16 FOR KEY)

Key to Figure 4

- A. One-half inch thick clear Pittsburgh plate glass window.
- B. Achromatic lens, 33m diameter, 100mm focal length.
- C. Achromatic microscope objective, 3mm focal length.
- D. Spectral wedge filter, 4-inch diameter, 180° segment.
(Optical Coating Laboratory, Inc.)
- E. Filter drive motor, Model 41-25, 42 rpm, 35 v reversible D.C.
(Hansen Manufacturing Co.)
- F. Photomultiplier tube (EMI 9524B).
- G. Electronic circuitry for PM tube.
- H. Burr-Brown Model 520/25, ± 15 volt dual regulator power supply.
- J. Mu-metal shield.
- K. Geared 26vdc motor, Globe Model C5A1106, reversible, 24,000rpm nominal with 4126:1 gear reducer, 500 oz-in maximum continuous torque.
- L. Geared 26 vdc motor, Globe Model C5A1092, reversible 24,000rpm nominal with 2273:1 gear reducer, 370 oz-in maximum continuous torque.
- M. Potentiometer, azimuth angle (ϕ), Model 130 SRD, 10K, 0.5% linearity. (Spectral Instrument Co.)
- N. Potentiometer, vertical angle (θ), Model 130 SRD, 10K, 0.5% linearity. (Spectral Instrument Co.)
- P. Reversing switches, DPDT.
- Q. Lead counterbalance weights.
- R. Stand.
- S. Junction Box.
- T. Aluminum Rudder (20 inches X 19 inches).
- U. Three-sixteenths inch, 4-conductor, externally armored, well logging cable.
- V. Mecca No. 2047 seven-pin underwater electrical connector.

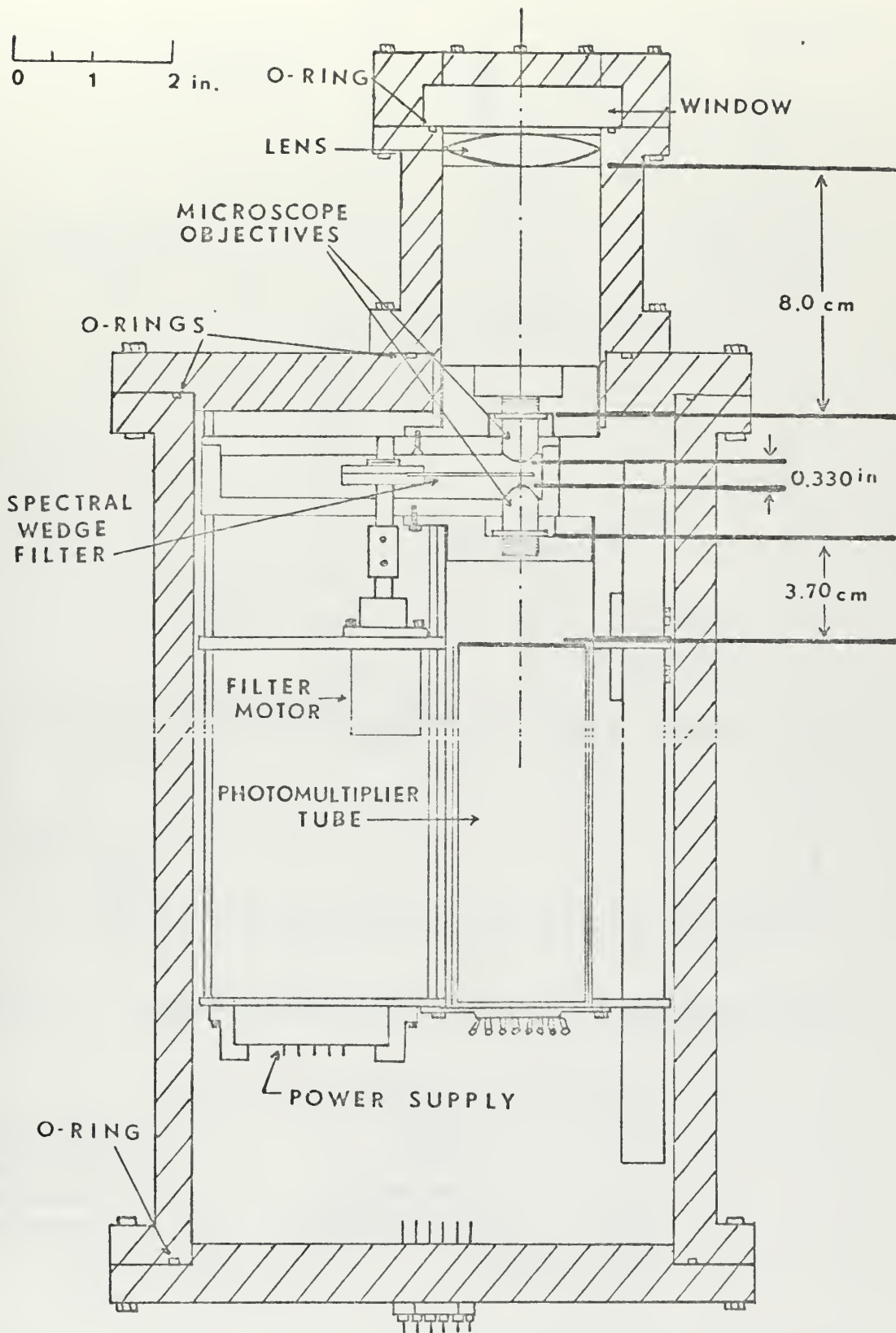


FIGURE 5. GENERAL ARRANGEMENT OF PHOTOMETER UNIT

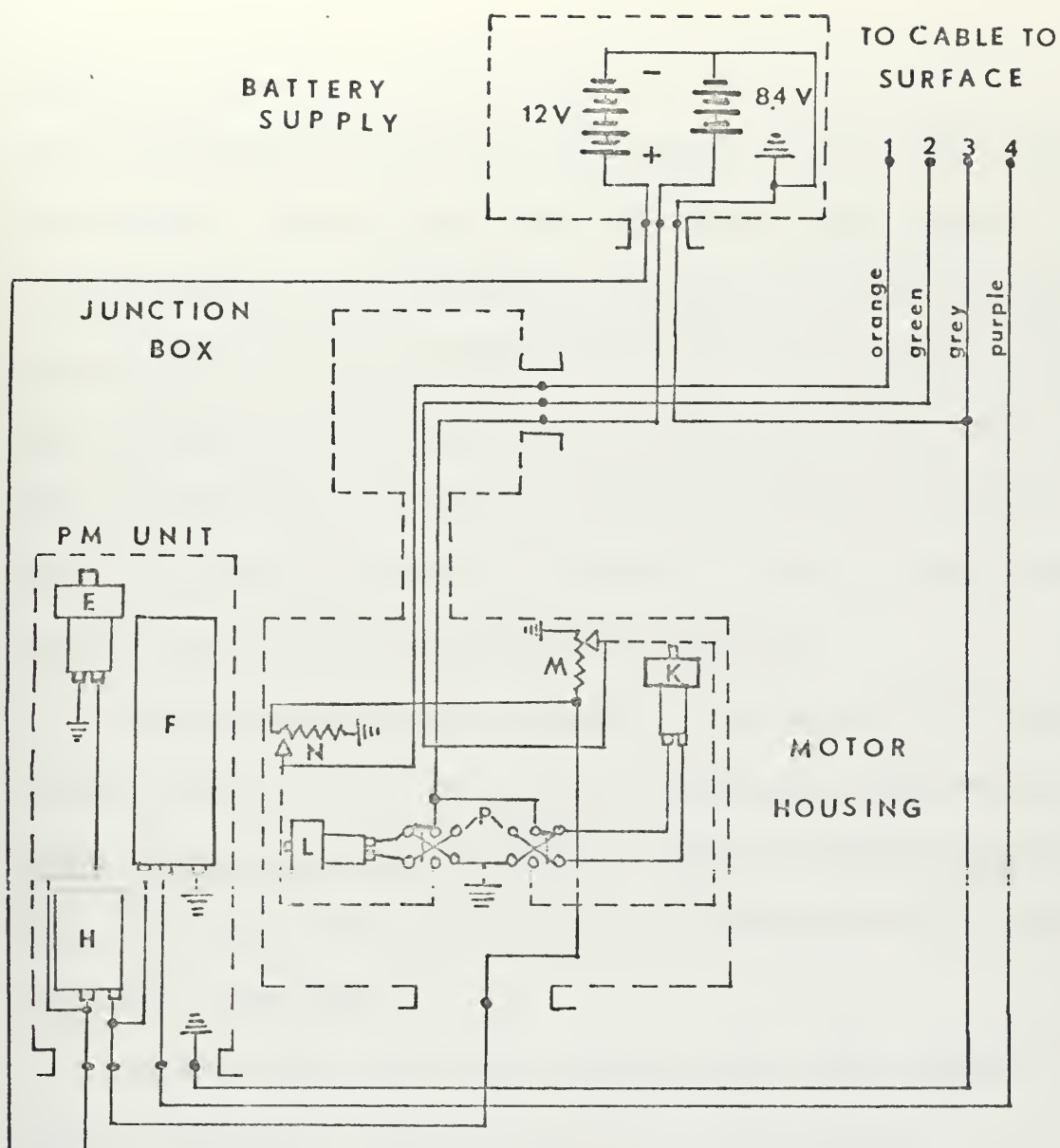


FIGURE 6. BLOCK ELECTRICAL DIAGRAM OF UNDERWATER UNIT

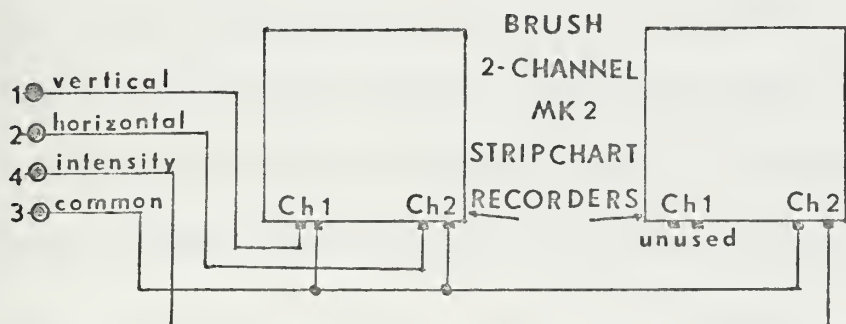


FIGURE 7. CIRCUIT DIAGRAM OF SHIPBOARD RECORDING SYSTEM
(SEE PAGE 16 FOR KEY)

allowing it to rotate 180° in a vertical plane while simultaneously rotating 360° in a horizontal plane. The optical system (Figure 5) allows light to enter through a 1/2-inch thick, clear, plate glass window within an angle of acceptance of 0.00119 steradians. Light passing through the achromatic objective lens ($f=100\text{mm}$) is collimated by an inverted achromatic microscope objective ($f=3\text{mm}$) before passing through the spectral wedge filter. After passing through the filter the rays are then diverged by another achromatic microscope objective, identical to the first, in order to spread the light beam over the photocathode of the detector.

A 4-inch diameter spectral wedge filter, manufactured by Optical Coating Laboratory, Inc., and having the transmission characteristics shown in Figure 8, is used. The filter is driven at 24 rpm by a small D.C. motor. Alignment of the optical system was accomplished on an optical bench with a neon laser.

The photometer circuitry was designed by Mr. Floyd Miller of the Visibility Laboratory of Scripps Institution of Oceanography, La Jolla, California. An 11-stage EMI 9524B high gain photomultiplier tube having a 0.91-inch window and S-11 response is employed. The photometer circuitry is illustrated in Figure 9, and graphs of the photomultiplier characteristics are shown in Figures 10 and 11. Operating power for the photomultiplier tube circuitry and the Burr-Brown Model 520/25, ± 15 vdc power supply maintains an output which is constant to within $\pm 0.25\%$ over the input voltages used. The photometer output signal, which varies from 0 to -10 vdc, is recorded at the surface on a two-channel strip-chart recorder.

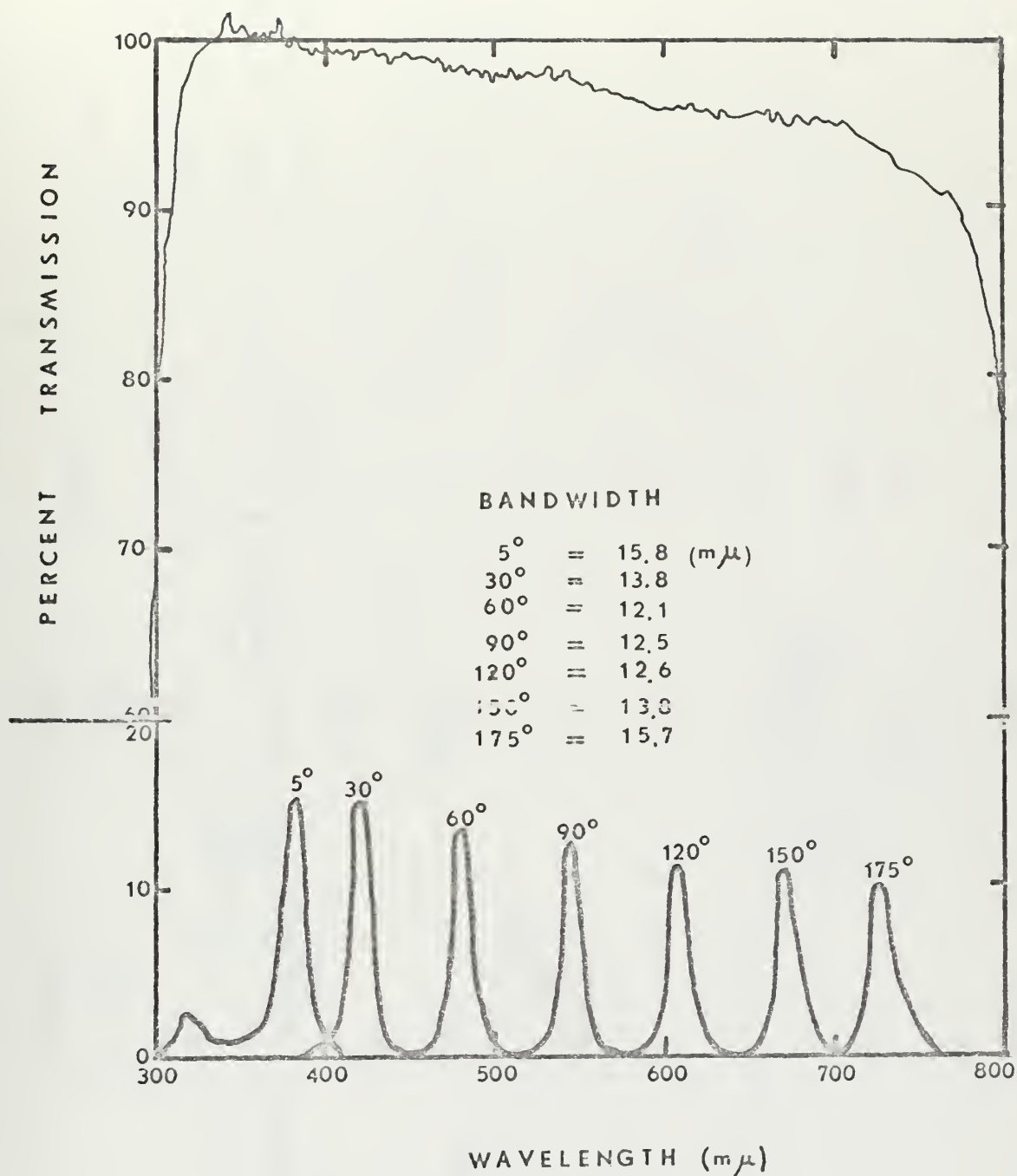


FIGURE 8. SPECTRAL WEDGE FILTER CHARACTERISTICS

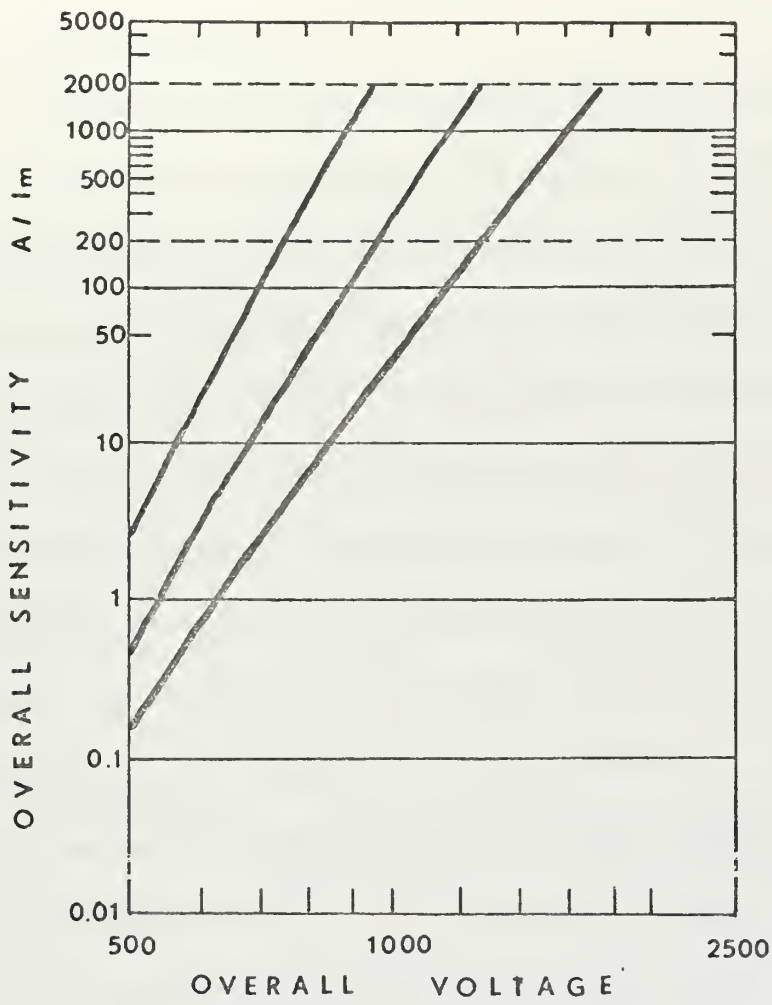


FIGURE 10. OVERALL SENSITIVITY VS OVERALL VOLTAGE

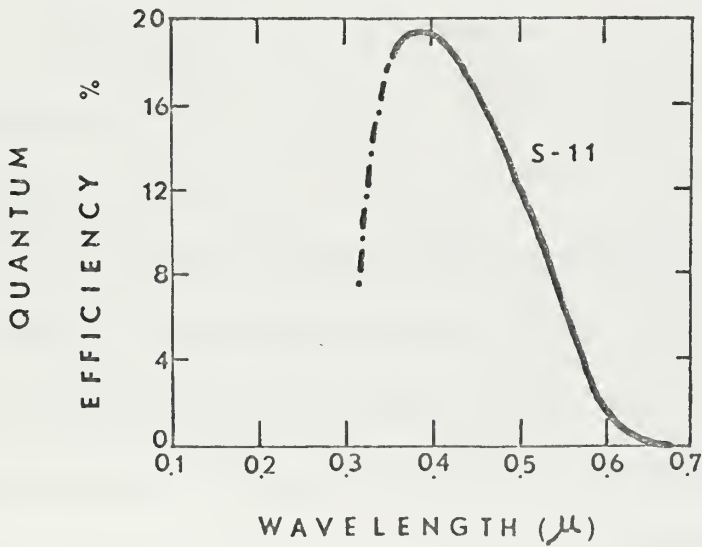


FIGURE 11. PHOTOMULTIPLIER TUBE SPECTRAL RESPONSE

2. Motor Housing Unit

The motor housing is constructed of stainless steel periscope stock having an internal diameter of 6 1/2 inches, a length of 8 inches, and 1/2-inch walls. The end plates are made of 3/4-inch aluminum. Brass bearings provide lateral support for the rotating stainless steel shafts. O-rings seal the shafts and end plates of the unit from the sea water. Inside the motor housing (Figure 4) are two reversible D. C. motors, azimuth (ϕ) and vertical (θ) angle potentiometers, and reversing switches, which provide for continuous photometer rotation through 180° in a vertical plane and 360° in a horizontal plane. The ϕ -shaft motor is driven at 5.33 degrees/second by a small 35 vdc motor while the θ -shaft is driven by another motor at 13.4 degrees/second. Angular rotations are measured with two potentiometers having 0.5% linearity, the outputs of which are displayed on a shipboard two-channel strip-chart recorder.

3. Junction Box

The junction box is constructed of 1/2-inch thick aluminum tubing having an internal diameter of 4 inches and length of 5 inches. The end plates are made of 3/4-inch aluminum. A hollow stainless steel shaft connects the motor housing to the junction box and provides a passage for electrical wires between the two units. To the junction box is attached a 20-inch by 19-inch rudder to stabilize the meter with respect to a vertical plane. The signals from the two angle potentiometers are brought out through two single-pin underwater connectors located at one end of the cylinder.

4. Battery Supply

The battery housing is 8 inches long with 3/4-inch end plates and is made of the same periscope stock used for the motor housing. Nickel-cadmium cells having 4 ampere-hour capacity are used in the battery packages. One package contains 10 cells (12v) and provides power to operate the spectral wedge filter motor, the photometer circuitry, and the angle potentiometers. The other package contains 7 cells (8.4 v) and provides operating power to the ϕ and θ drive shafts.

B. CALIBRATION

1. Azimuth and Vertical Angles

A Lietz three-arm vernier protractor and a Brush two-channel strip-chart recorder were used to measure chart line deflection as a function of angular rotation in the vertical and horizontal planes. Calibration curves for azimuth and vertical angles are shown in Figures 12, 13, and 14.

2. Spectral Wedge Filter

Narrow-band interference filters were used with sodium and mercury arc lamps in the calibration of the spectral wedge filter for wavelengths as a function of angle of rotation. The only sodium line used was that at 589.0 nm, while the mercury lines used were at 404.66, 435.84, 546.10, 578.02 and 690.72 nm. Figure 15 gives transmission wavelength of the wedge filter as a function of angle of rotation.

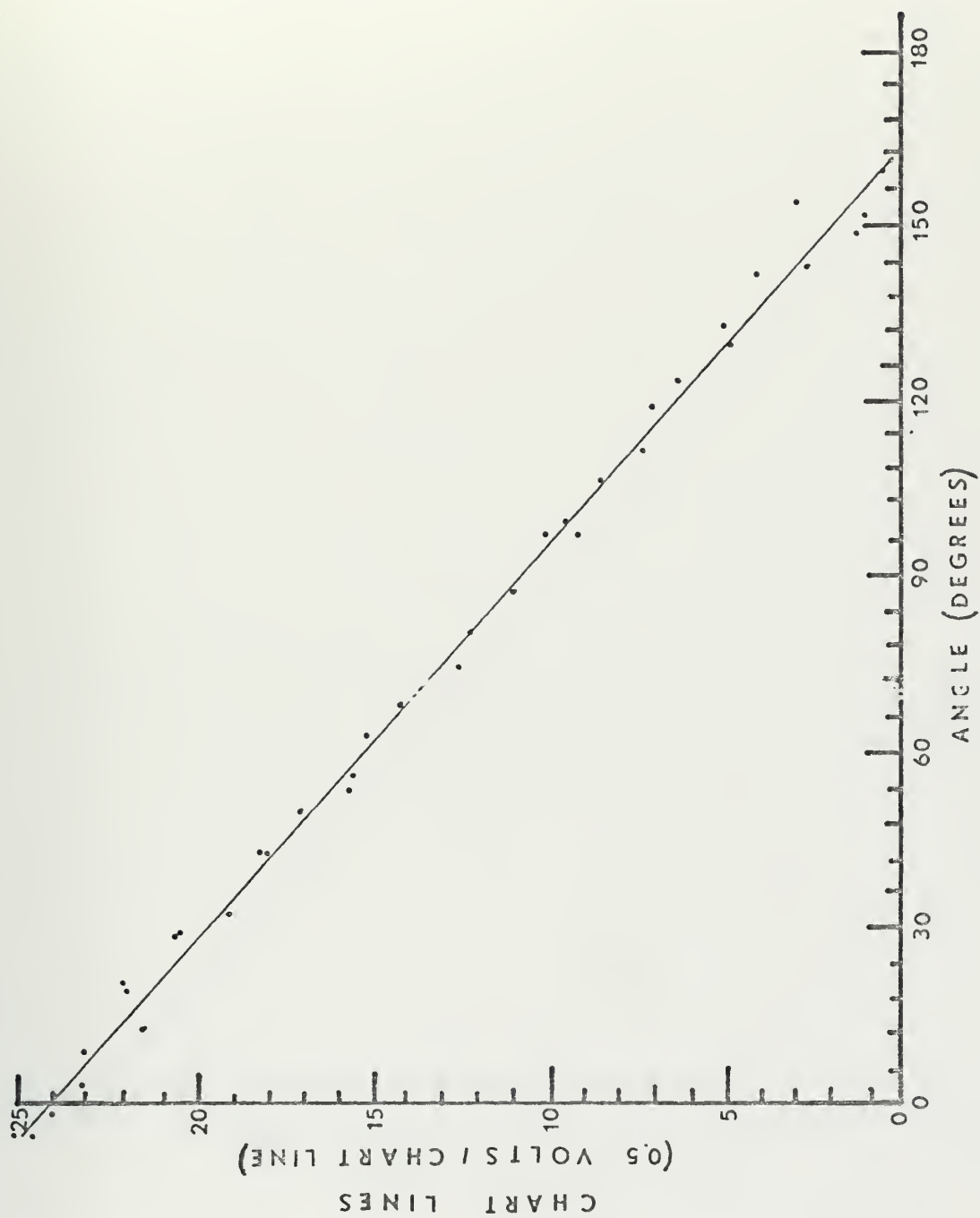


FIGURE 12. VERTICAL ANGLE CALIBRATION CURVE IN DOWNWARD DIRECTION

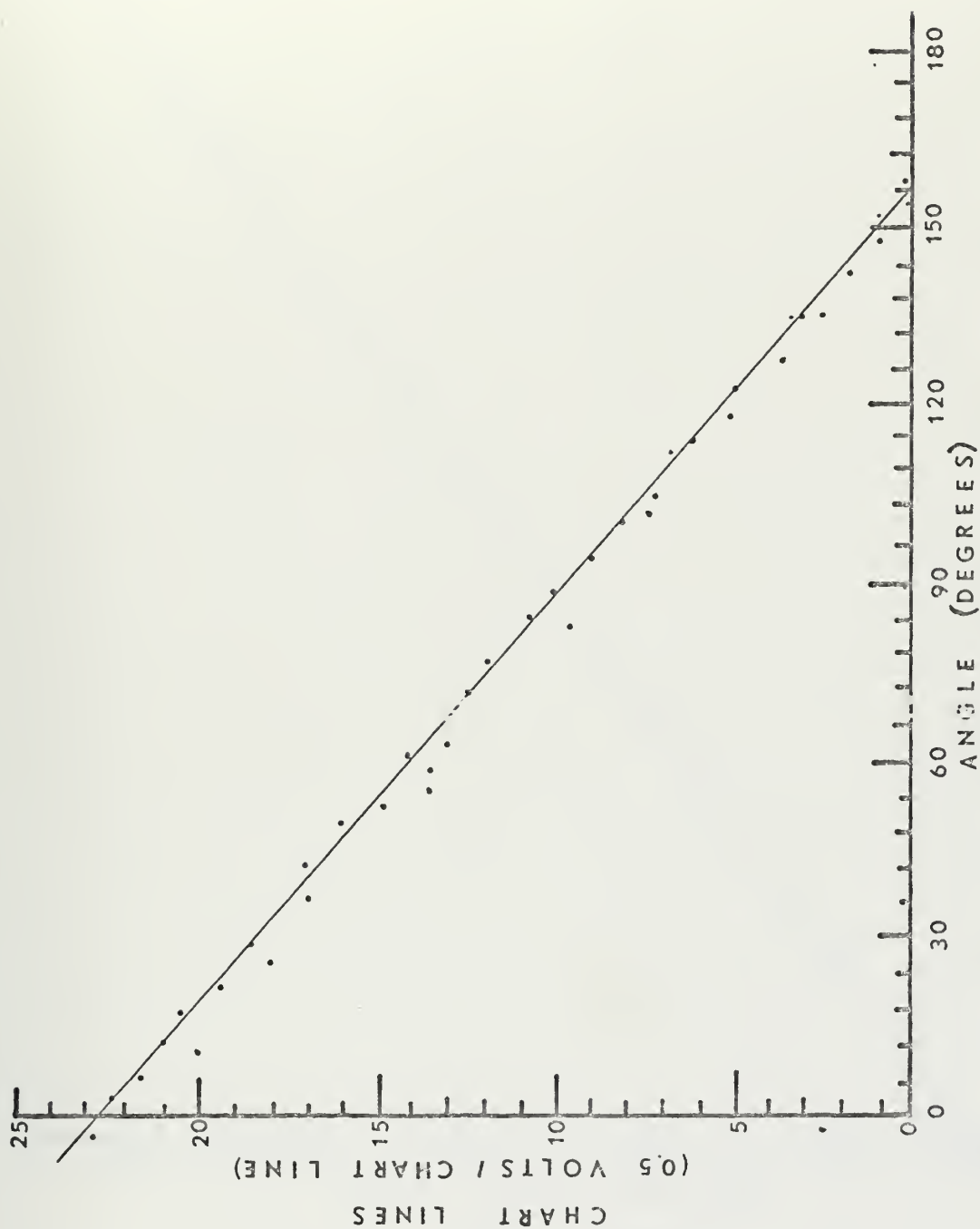


FIGURE 13. VERTICAL ANGLE CALIBRATION CURVE IN UPWARD DIRECTION

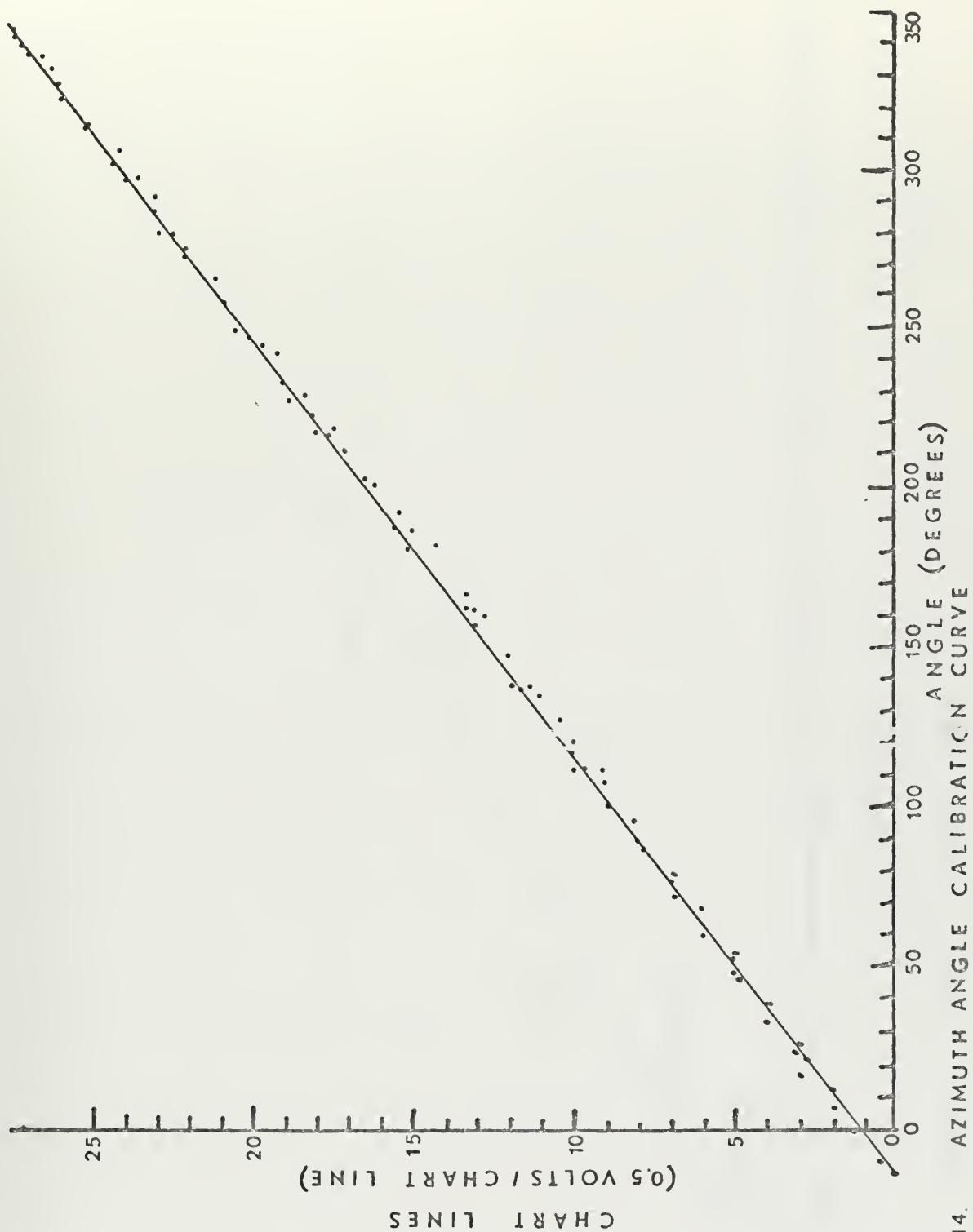


FIGURE 14.

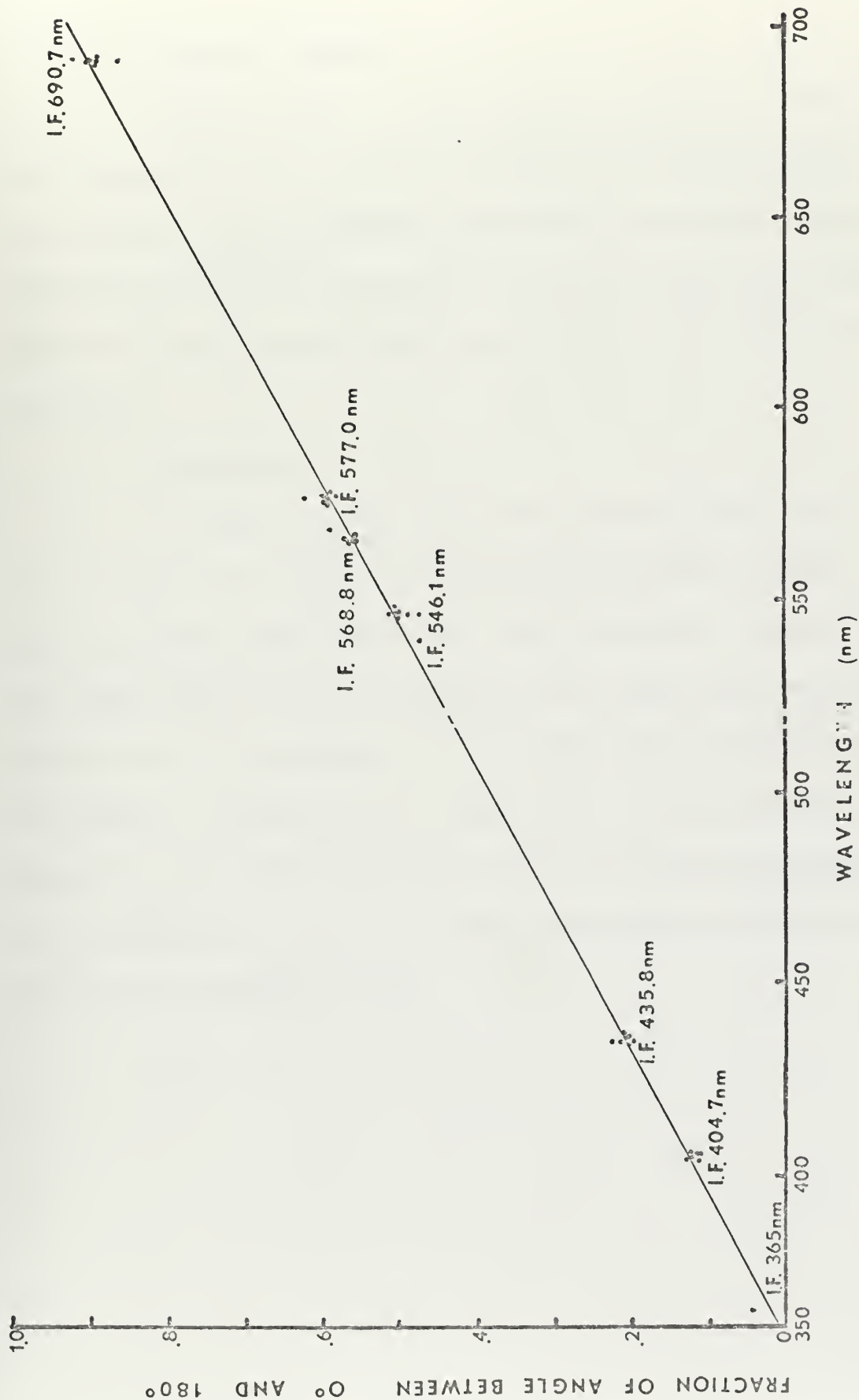


FIGURE 15. SPECTRAL WEDGE FILTER ROTATION CALIBRATION CURVE

3. Acceptance Angle

A He-Ne laser ($\lambda = 632.8 \text{ nm}$) was used with a neutral density filter to measure the acceptance angle of the photometer (Figure 16). The photometer unit was rotated at small angular increments, and radiance (chart line deflection) was recorded as a function of half-angle rotation (Figure 17). The acceptance angle was determined to be $2^\circ 14'$ or 0.00119 steradians.

4. Photometer

A Gamma Scientific Model 220 calibrated optical source system with a Model 220-1A radiance head was used in absolute intensity calibration of the photometer (Figure 18). The Model 220-1A radiance head has a light output of 100 ± 2 footlamberts, color temperature equal to $2854 \pm 50^\circ\text{K}$, and a uniformity of $\pm 1.5\%$ within the 3-inch diameter luminous surface. The Model 220-1A output curve is shown in Figure 19. Wratten No. 96 neutral density filters were used in density increments of 0.1 to calibrate the photometer in terms of intensity and wavelength in absolute units (Figures 32 - 44).

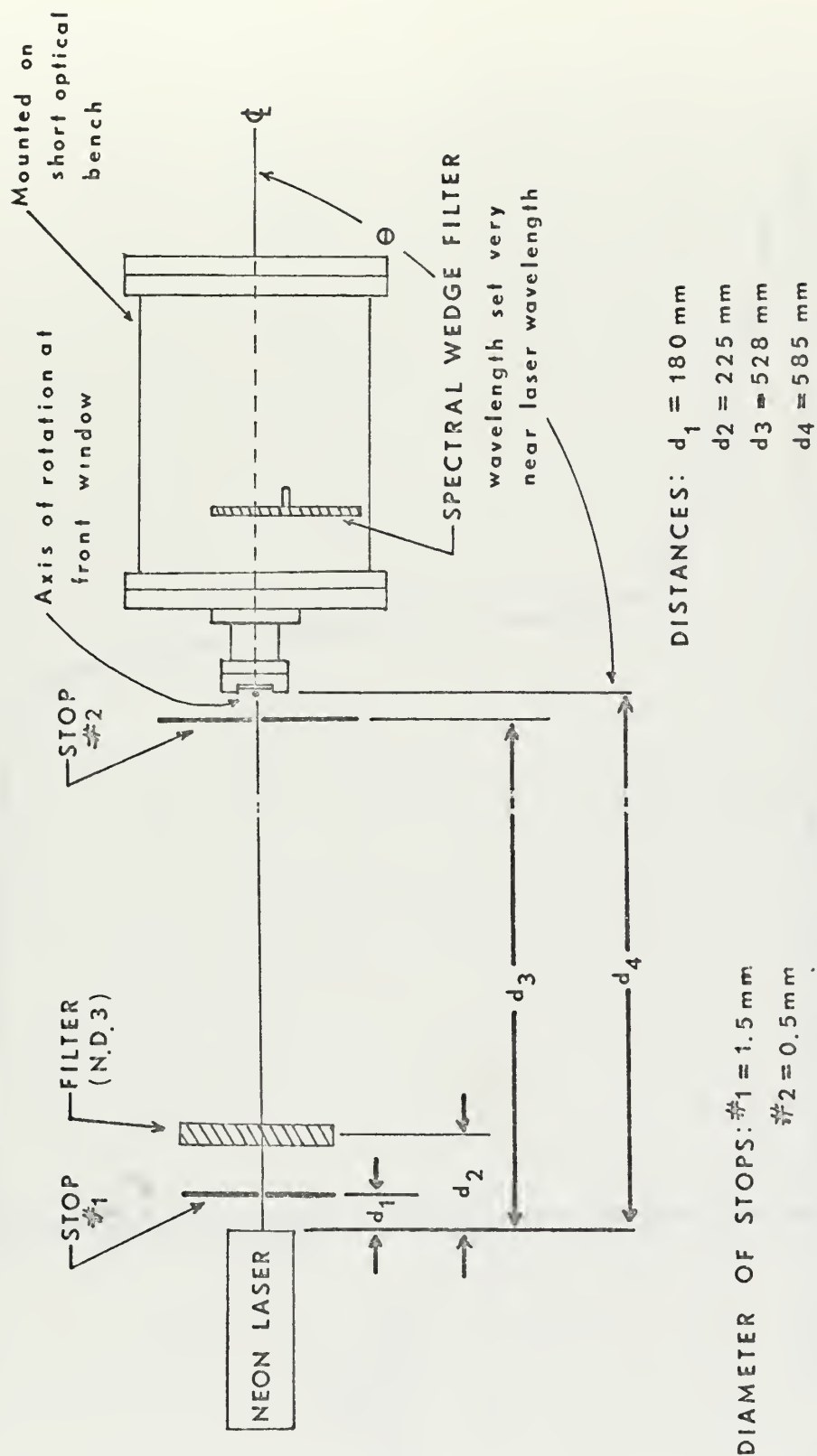


FIGURE 16. ACCEPTANCE ANGLE CALIBRATION ARRANGEMENT

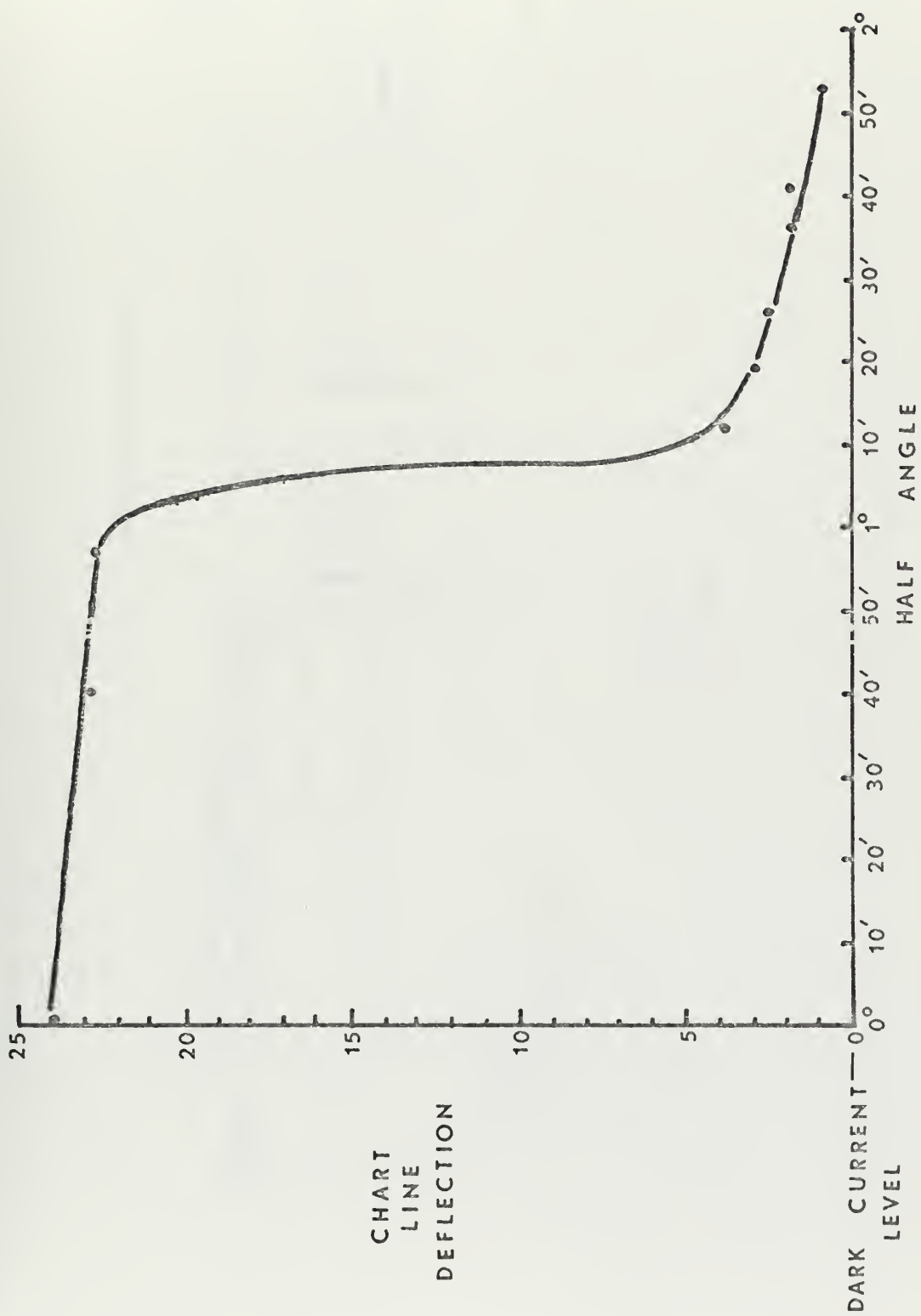


FIGURE 17. ACCEPTANCE ANGLE CALIBRATION CURVE

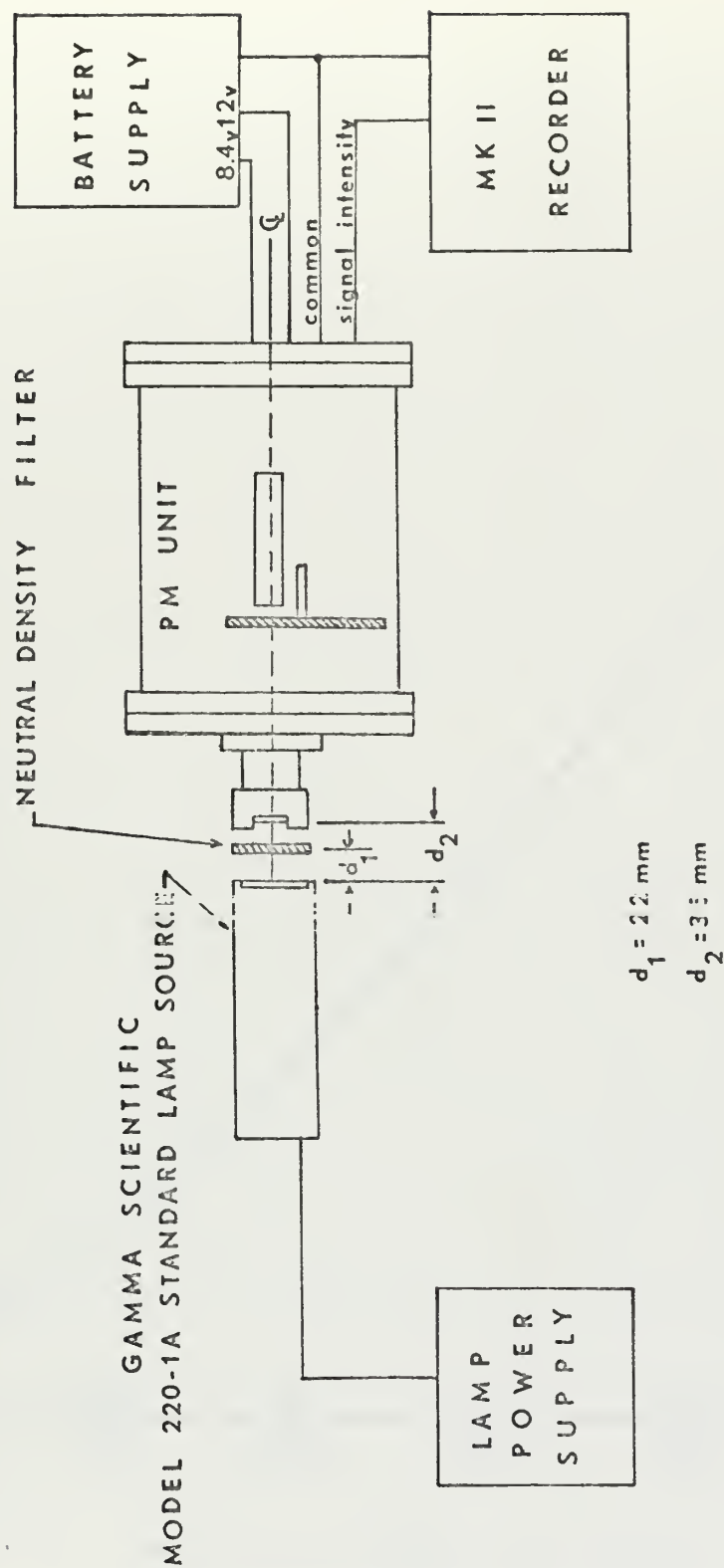


FIGURE 18. SYSTEM CALIBRATION ARRANGEMENT

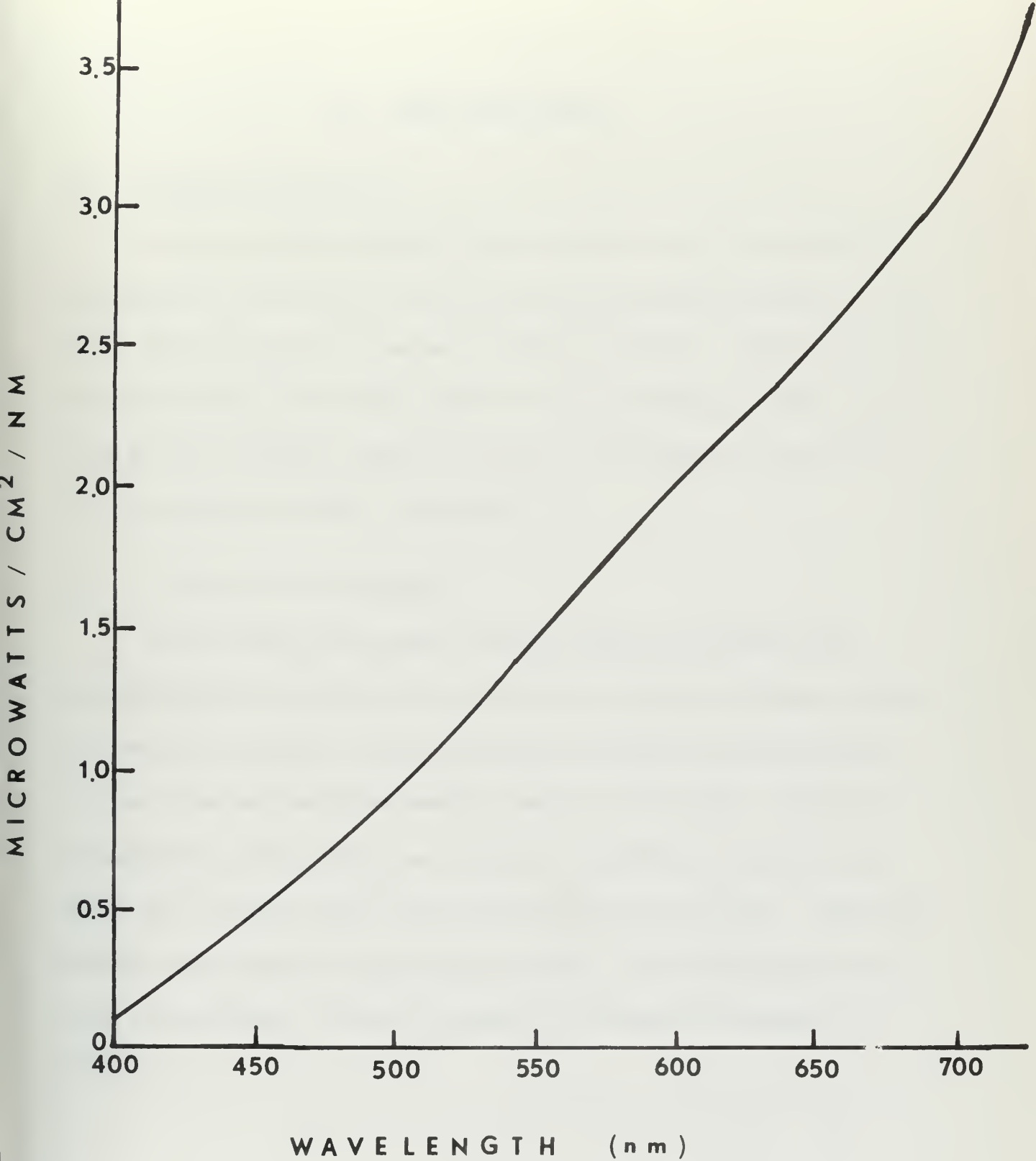


FIGURE 19. CALIBRATION CURVE FOR STANDARD LAMP

III. DATA COLLECTION

A. STATION LOCATIONS

During July 1971 spectral radiance measurements were made in Monterey Bay, California, aboard the Naval Postgraduate School's 63-foot boat. The two stations occupied are shown in Figure 1. Station positions were determined every fifteen minutes by visual bearings. These, along with the time, weather, altitude of the sun, and azimuth of the sun for each station are presented in Appendix C.

B. OPERATIONAL PROCEDURES

At each station the spectral radiance meter was lowered to the desired depths by means of a four-conductor, externally armored, electrical cable and allowed to rotate continuously through several rotational cycles in the horizontal and vertical planes at each depth. Continuous measurements of the angular and spectral distribution of submarine daylight were recorded on two dual-channel strip-chart recorders. Instrument depths were indicated by meter wheel readings. The wire angle for each case was negligible. Typical recordings of raw data are presented in Figure 20.

DEPTH

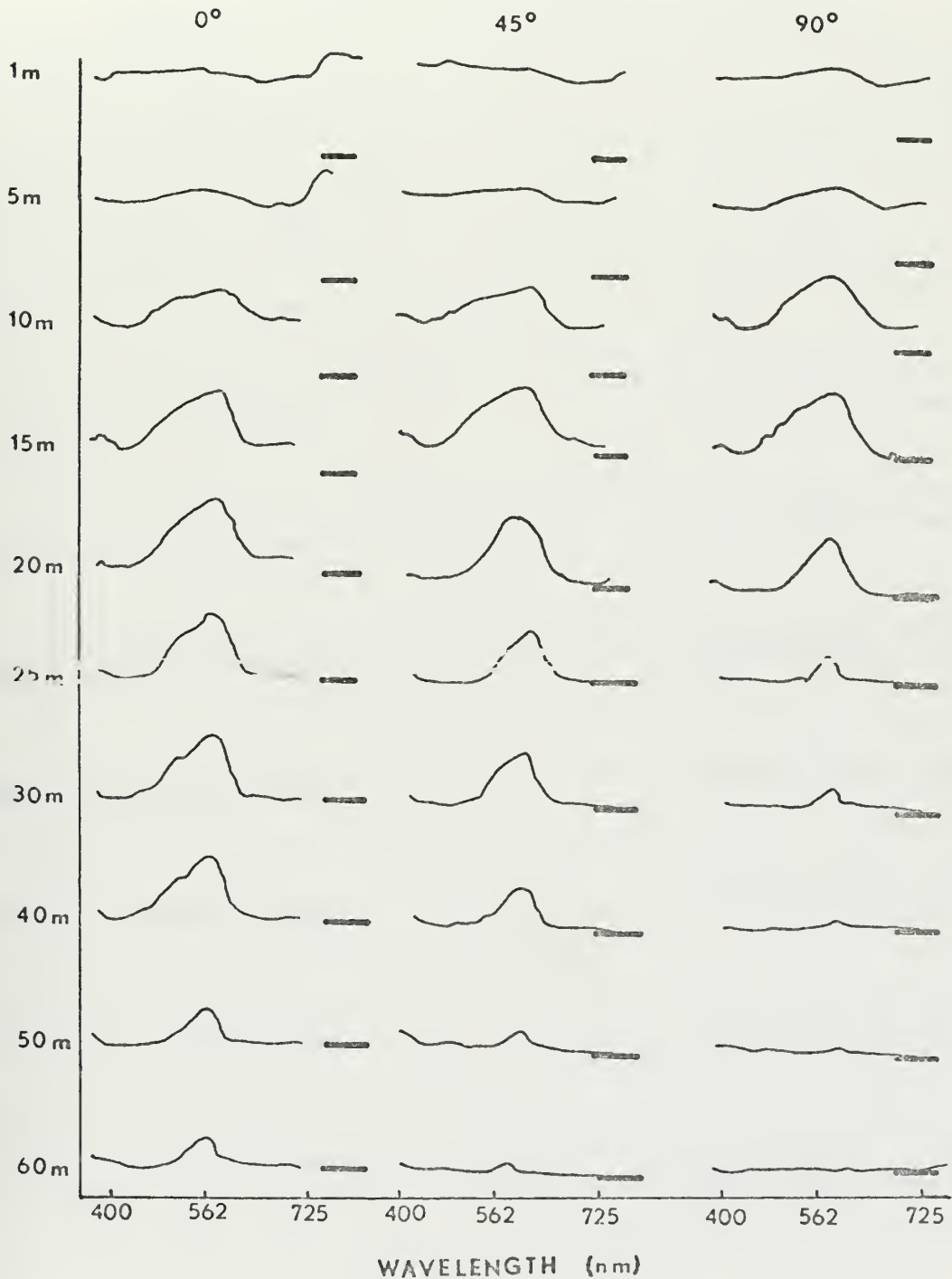
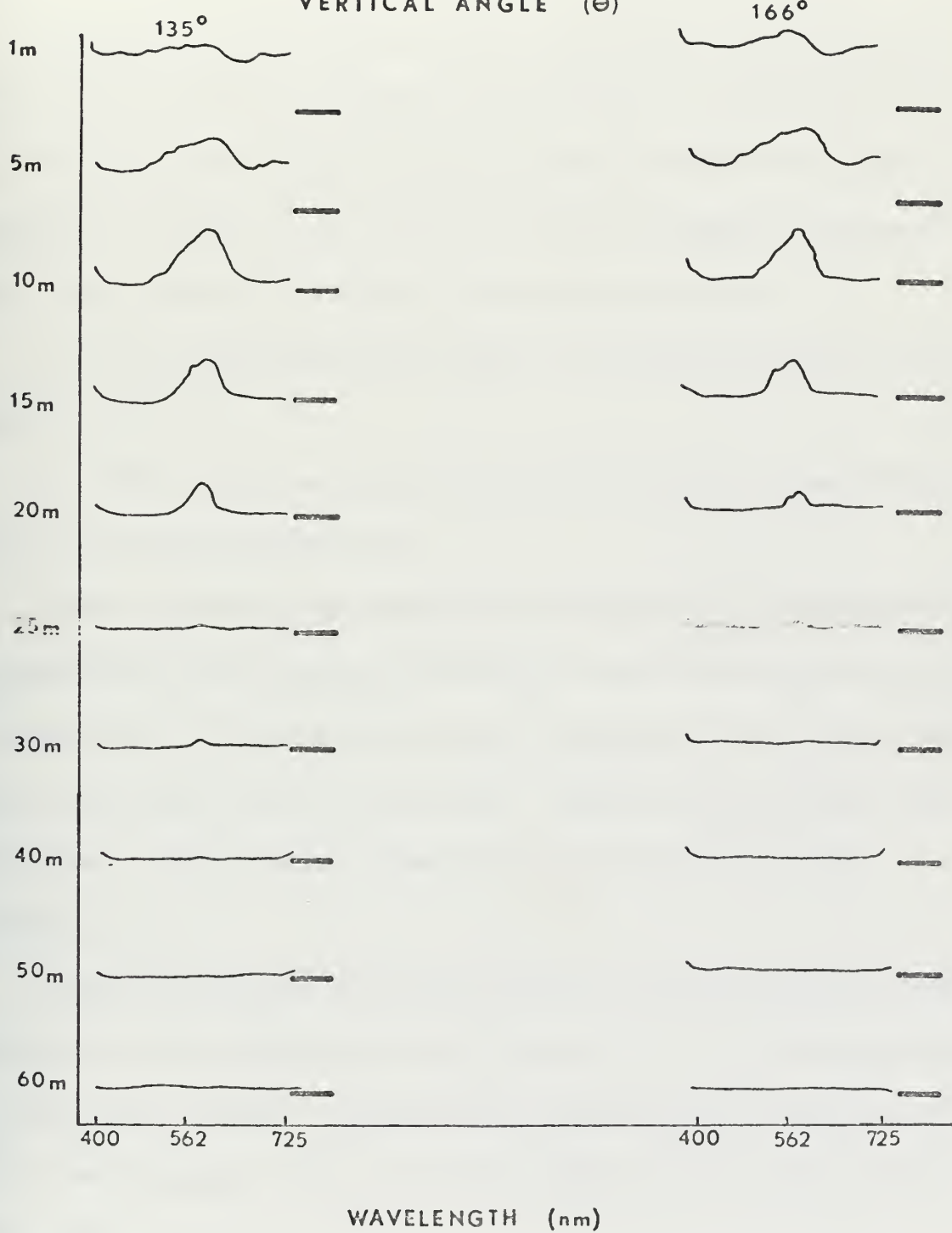
VERTICAL ANGLE (θ)

FIGURE 20. UNCORRECTED SPECTRAL RADIANCE VARIATION WITH DEPTH AT $\phi = 0$. THE DARK CURRENT REFERENCE LEVEL IS INDICATED TO THE RIGHT OF EACH CURVE.

DEPTH

VERTICAL ANGLE (θ)



IV. DATA ANALYSIS

A manual analysis of the uncorrected strip-chart records (Figure 21) was made, and values of absolute spectral radiance are shown in Appendix C. Using these data graphs of spectral radiance variation with depth were plotted for $\phi = 0$ and $\theta = 0, 45, 90, 135,$ and 166 degrees (Figures 22-31). In the analysis the following assumptions were used:

(1) The maximum intensity of light in the horizontal plane is in the azimuth of the sun.

(2) The vertical and horizontal axes of the meter remained stationary at a given depth during scans.

Angular rotation in the vertical and horizontal planes was determined by measuring vertical chart line deflections on the recorder output and then entering Figures 12-14 with these values to obtain the azimuth and vertical angle of a selected point of observation. Observed azimuth angles were expressed in relative angles to the direction of the sun by applying assumption (1).

Since the spectral wedge filter revolves at a constant angular speed, wavelength can be expressed in terms of time, $\lambda = \lambda(t)$, and recorded on the strip-chart recorder. Wavelength was then determined from the ratio of the partial angular rotation to the total angular rotation of the spectral wedge filter (Figure 15).

As shown in Figure 21, the spectral output shows the radiance of unfiltered light (high light levels) followed by spectral radiance (low light

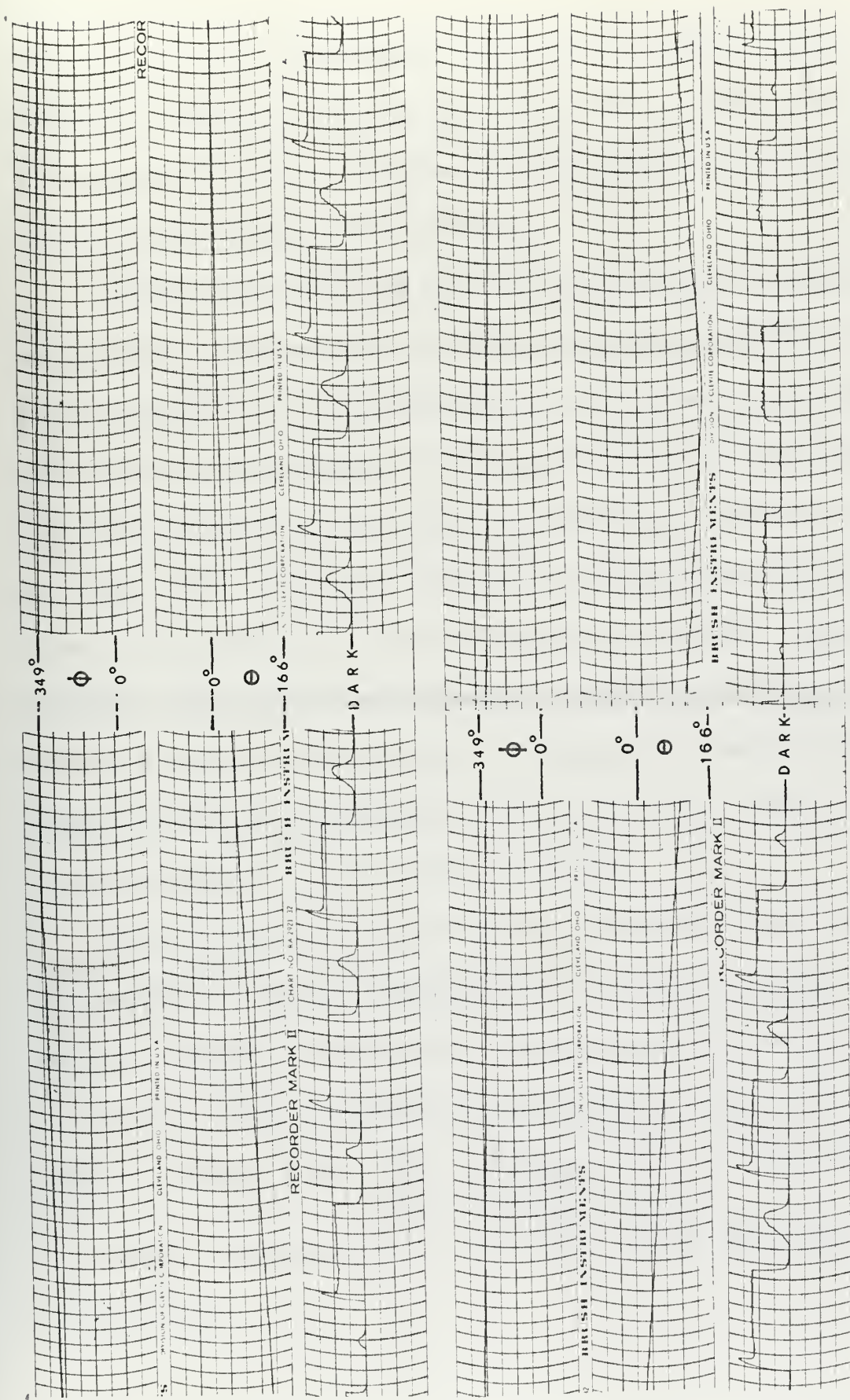


FIGURE 21. SAMPLE OF SPECTRAL RADIANCE OUTPUT

levels) from 350 to 725 nm, which is followed by unfiltered light. The end points of 0° and 180° on the spectral wedge filter are shown clearly as the sharp vertical lines. Overshooting of the curve is due to the rapid transition from filtered to unfiltered light.

Radiance was determined for the angle of acceptance of the meter by using the nomograms shown in Figures 32-44 (Appendix B). Measurements of vertical chart line deflections of the recorder output signal were converted to a corresponding intensity expressed by the neutral density filter used in the photometer system calibration for a selected wavelength band (Curve A). Radiance for the given wavelength band was then determined by using Curve B. Curve B represents a plot of the values of irradiance (Figure 19) of the standard lamp source over a 25 nm wavelength band as a function of transmittance. To express the spectral radiance in terms of $\text{W/cm}^2/\text{sr}$, a multiplying factor of 838.22 was applied to account for the acceptance angle of 0.00119 steradians.

When these figures were prepared the different Fresnel light reflection coefficients at normal incidence between the observational case (water and glass) and the calibration case (air and glass) were not taken into account. Thus the radiance values presented in the figures are all high by a constant factor, $\frac{n_{\text{air}}}{n_{\text{sw}}} \cdot \left(\frac{n_{\text{glass}} + n_{\text{sw}}}{n_{\text{glass}} + n_{\text{air}}} \right)^2$, where the n's are the indices of refraction for air, sea water, and the glass window used for the meter.

Figures 22-31 (Appendix A), which are plots of the spectral radiance distribution with depth, $\theta = 0, 45, 90, 135$, and 166 degrees at $\phi = 0$ degrees, show spectral peaks at about 570 nm. Peaks at about this wavelength were observed at Lake San Vicente by Tyler and Smith [1970] .

The figures also show an apparent high radiance in the 400 - 450 nm region which is probably instrumental in nature and due to the relatively slow recovery time of the photometer when subjected to sudden large steps in light intensity during filter rotation from unfiltered to filtered light. A similar feature is observed following the overshooting in the curves from filtered to unfiltered light (Figure 21).

In many of the figures the plots of spectral radiance at $\theta = 0$ and 45 degrees for shallow depths were not drawn because the radiant intensity in these regions exceeded the limitations of the standard lamp used in the photometer calibration.

V. CONCLUSIONS

A spectral radiance meter having a spectral wedge filter was designed, constructed and used to obtain measurements of spectral radiance with depth at two stations in southern Monterey Bay, California, on an overcast day. Variations of the spectral radiance distribution with depth were plotted for the following vertical angles (θ): 0, 45, 90, 135, and 166 degrees. The azimuth angle (ϕ) was zero degrees with respect to the sun. The results seem reasonable in all cases.

A rotating spectral wedge filter is a practical means of obtaining a spectral radiance response.

The manner in which data was recorded imposed severe limitations on analysis. In future studies the radiance meter will be wired directly to the multiplexer and A-to-D converter of a PDP-8/S computer. This will greatly simplify the problem of data handling.

It is recommended that horizontal and vertical reference sensors be installed to improve the accuracy of the results.

Its size and shape make the instrument convenient for performing frequent observations, and future studies with this instrument are planned. In future research, simultaneous measurements of transmissivity, scattering and spectral radiance will be made in Monterey Bay to provide sufficient empirical data to test the theoretical laws of light distribution in the sea. In addition, the meter will be used in base-line studies of California coastal waters.

APPENDIX A

Figures of Spectral Radiance Distribution with Depth at $\phi = 0^\circ$ and $\theta = 0, 45, 90, 135, \text{ and } 166^\circ$ for Stations 1 and 2.

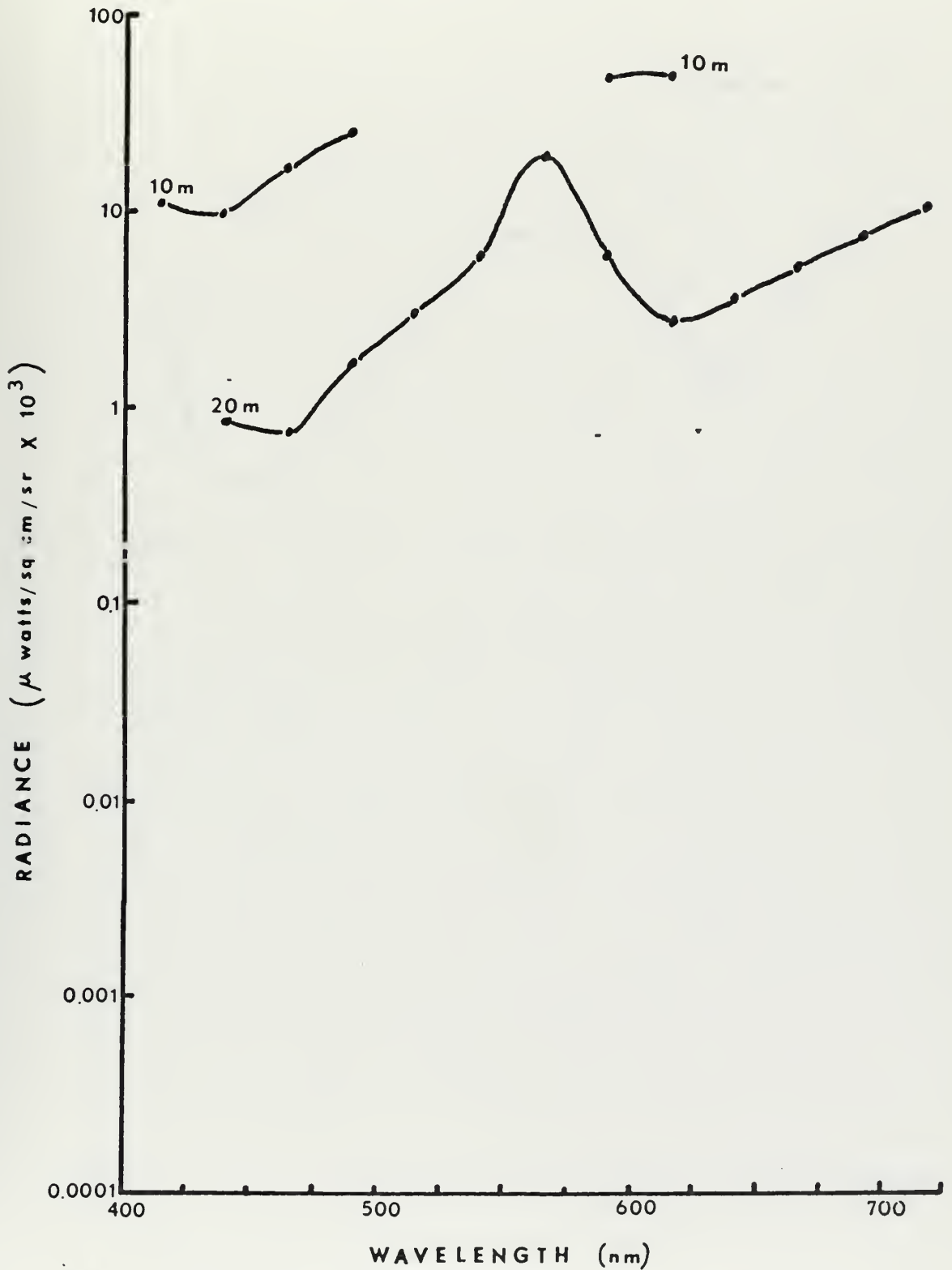


FIGURE 22. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\theta = 0^\circ$ AND $\phi = 0^\circ$, STA 1

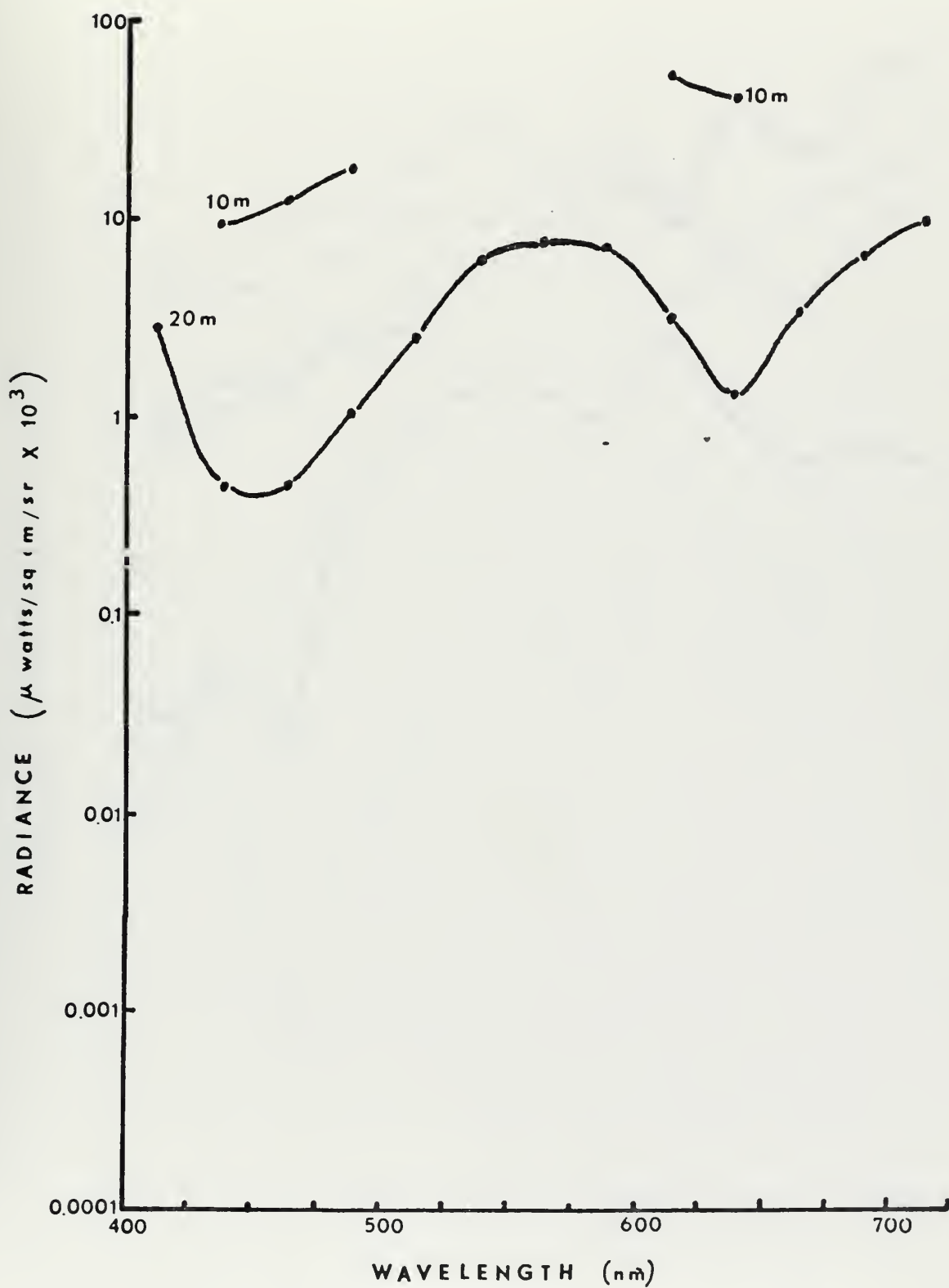


FIGURE 23. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\theta = 45^\circ$ AND $\phi = 0^\circ$, STA 1

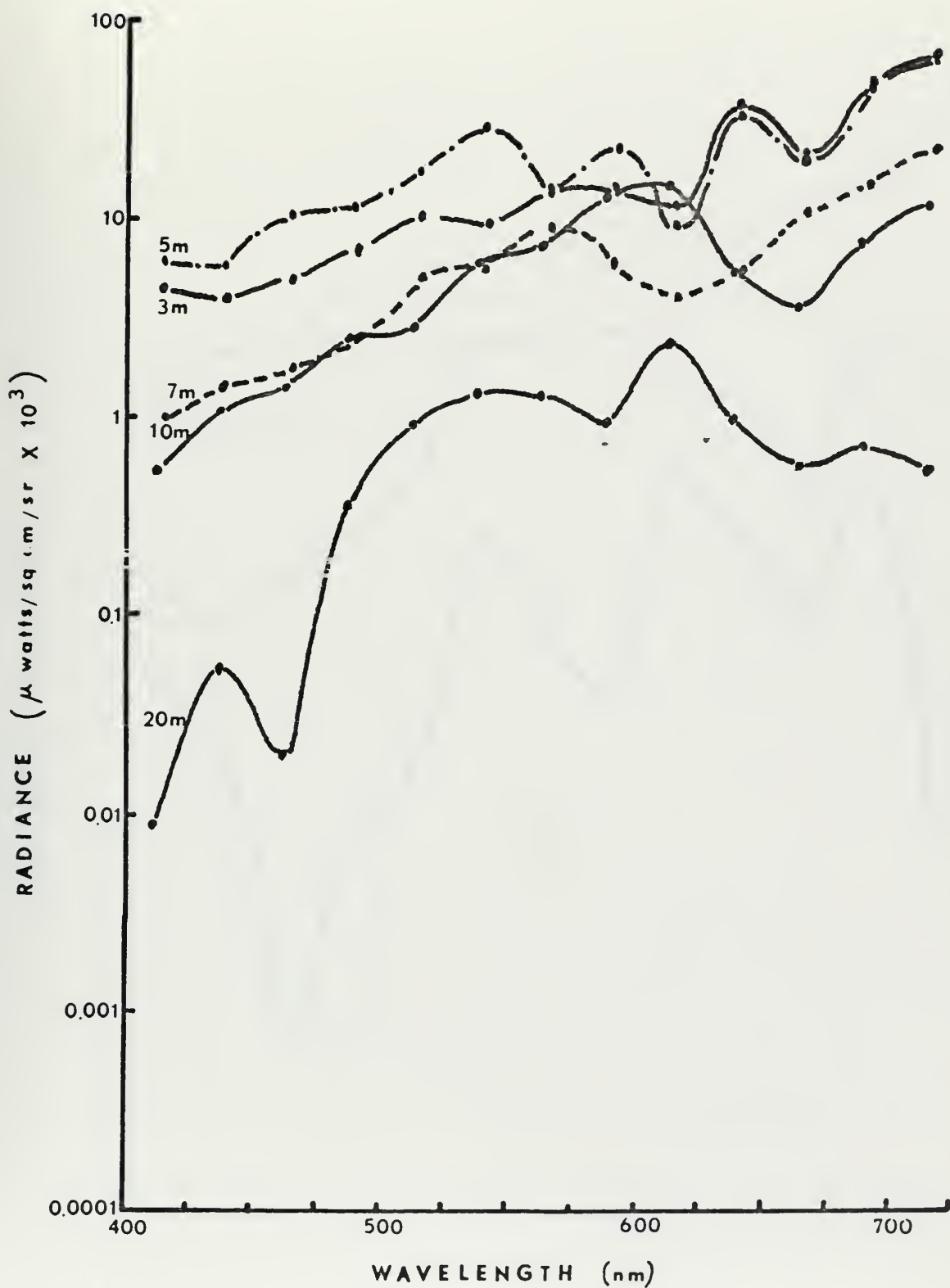


FIGURE 24. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\theta = 90^\circ$ AND $\phi = 0^\circ$, STA 1

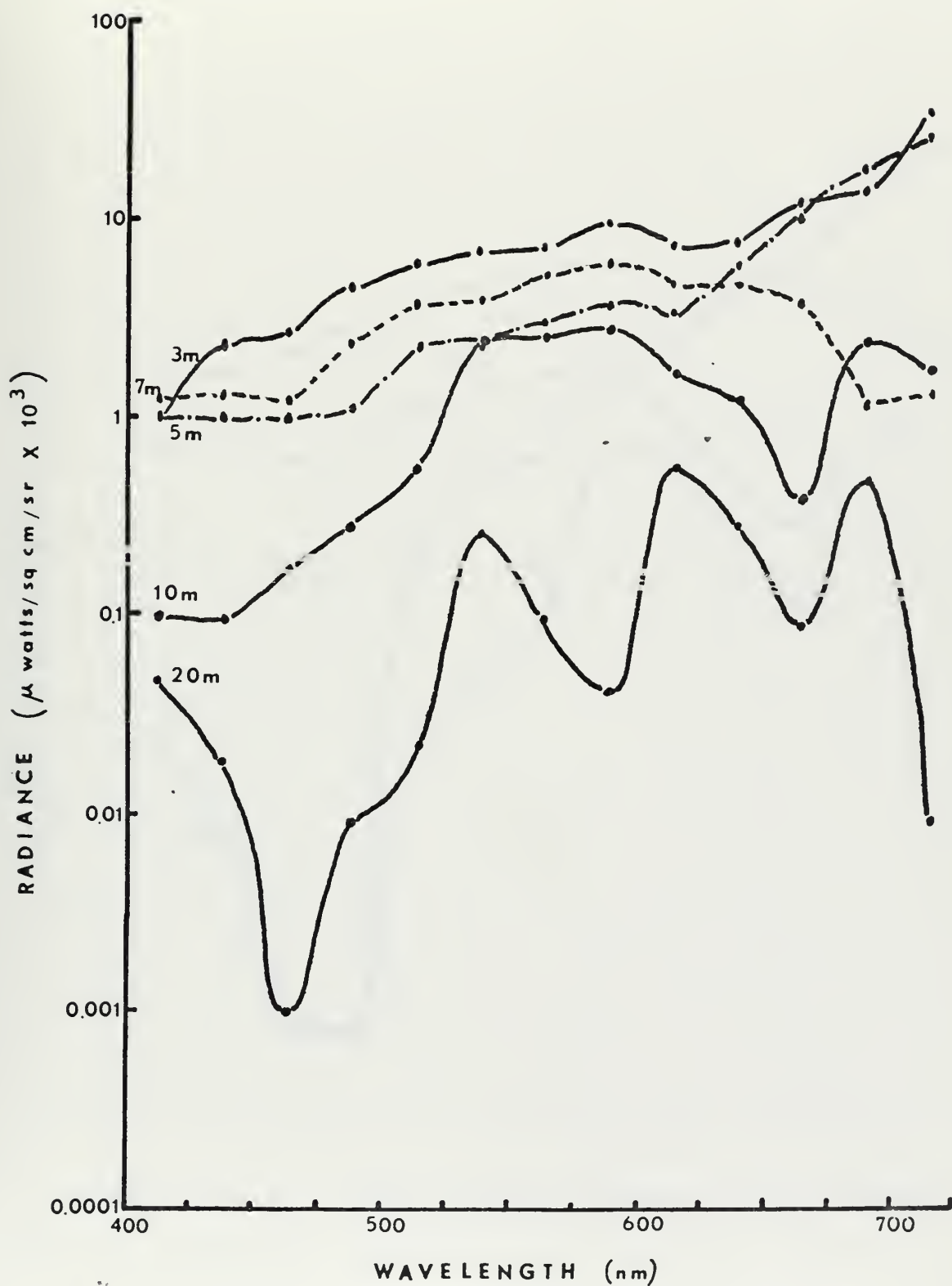


FIGURE 25. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\theta = 135^\circ$ AND $\phi = 0^\circ$, STA 1

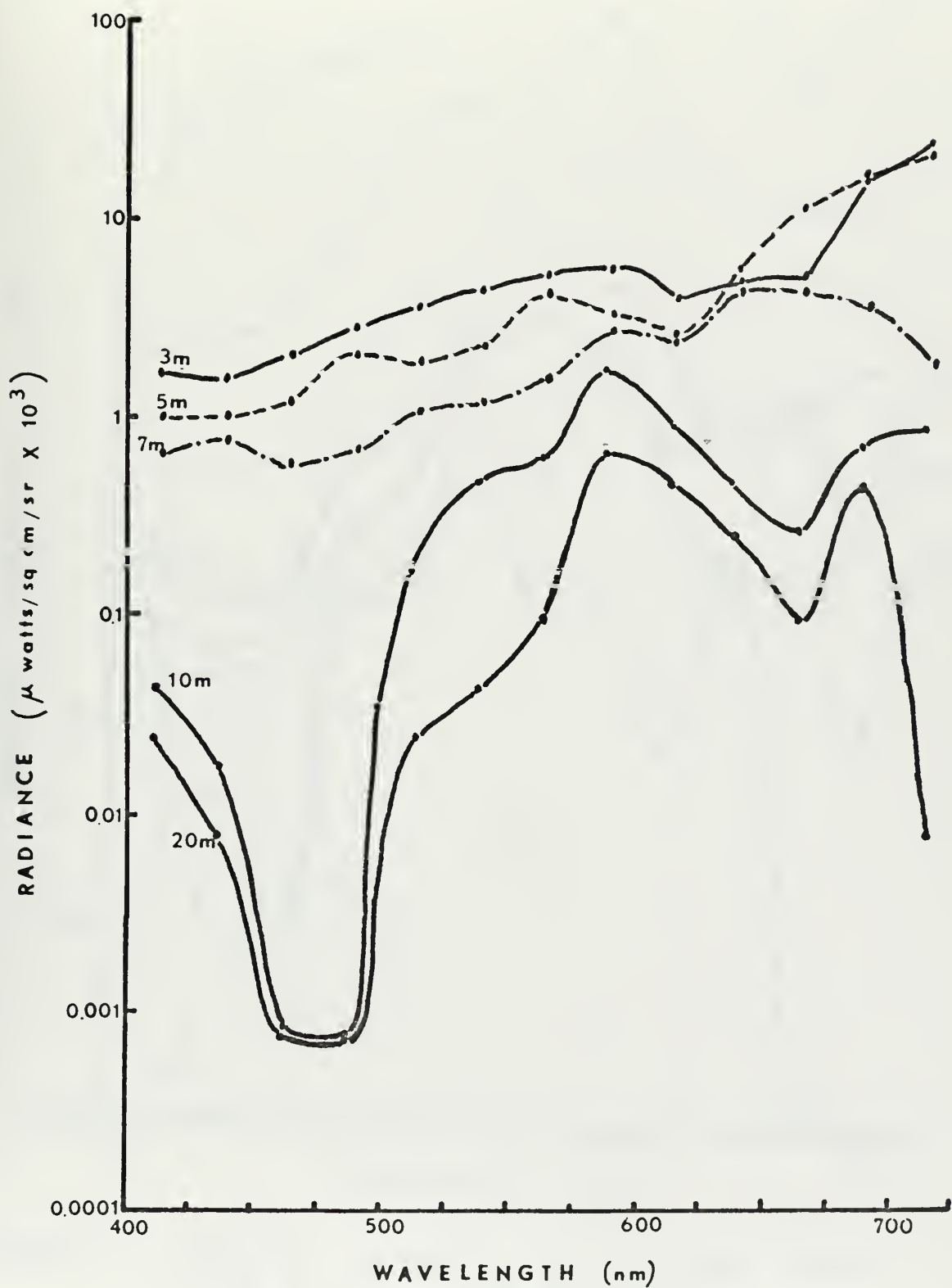


FIGURE 26. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\theta = 166^\circ$ AND $\phi = 0^\circ$, STA 1

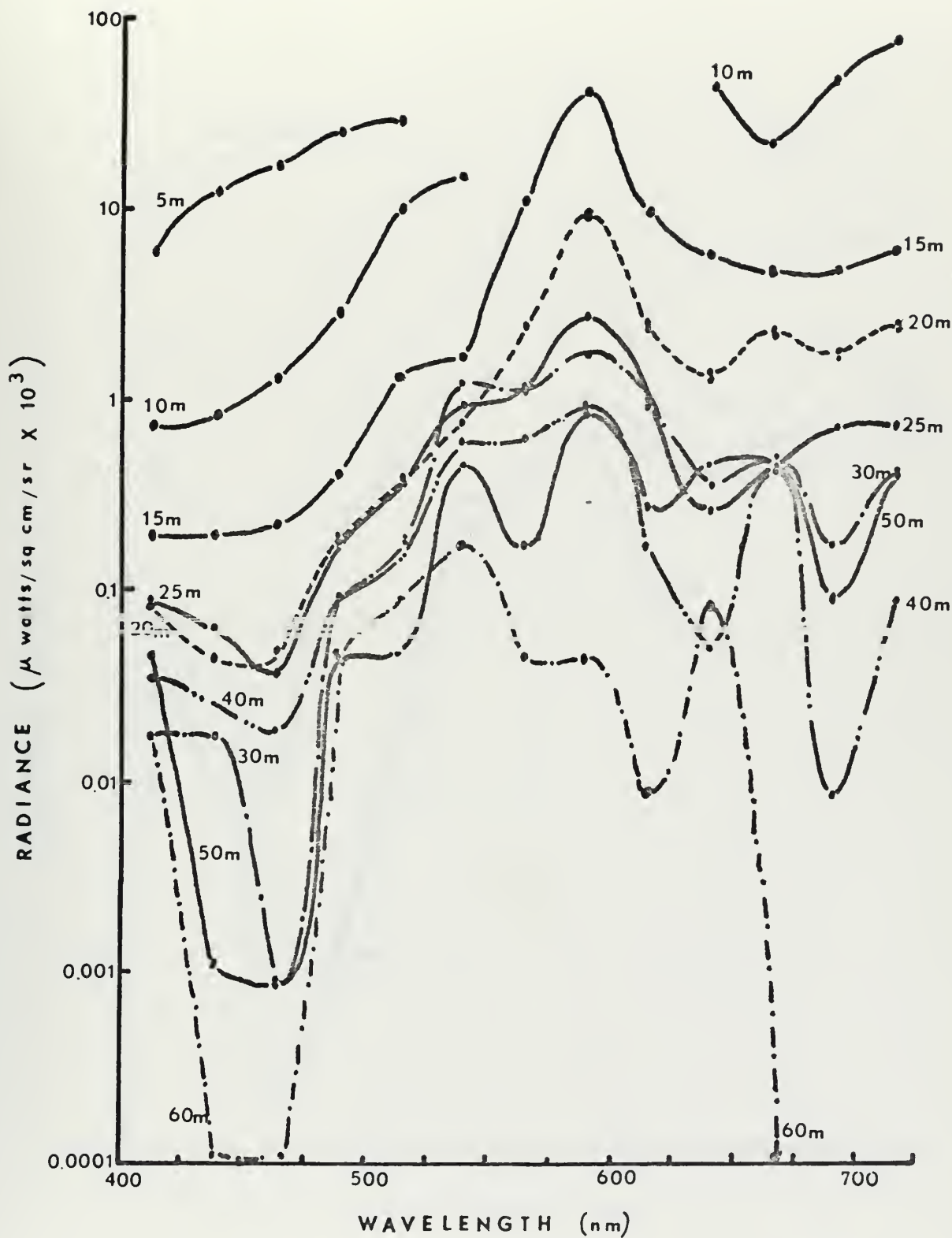


FIGURE 27. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\Theta = 0^\circ$ AND $\phi = 0^\circ$, STA 2

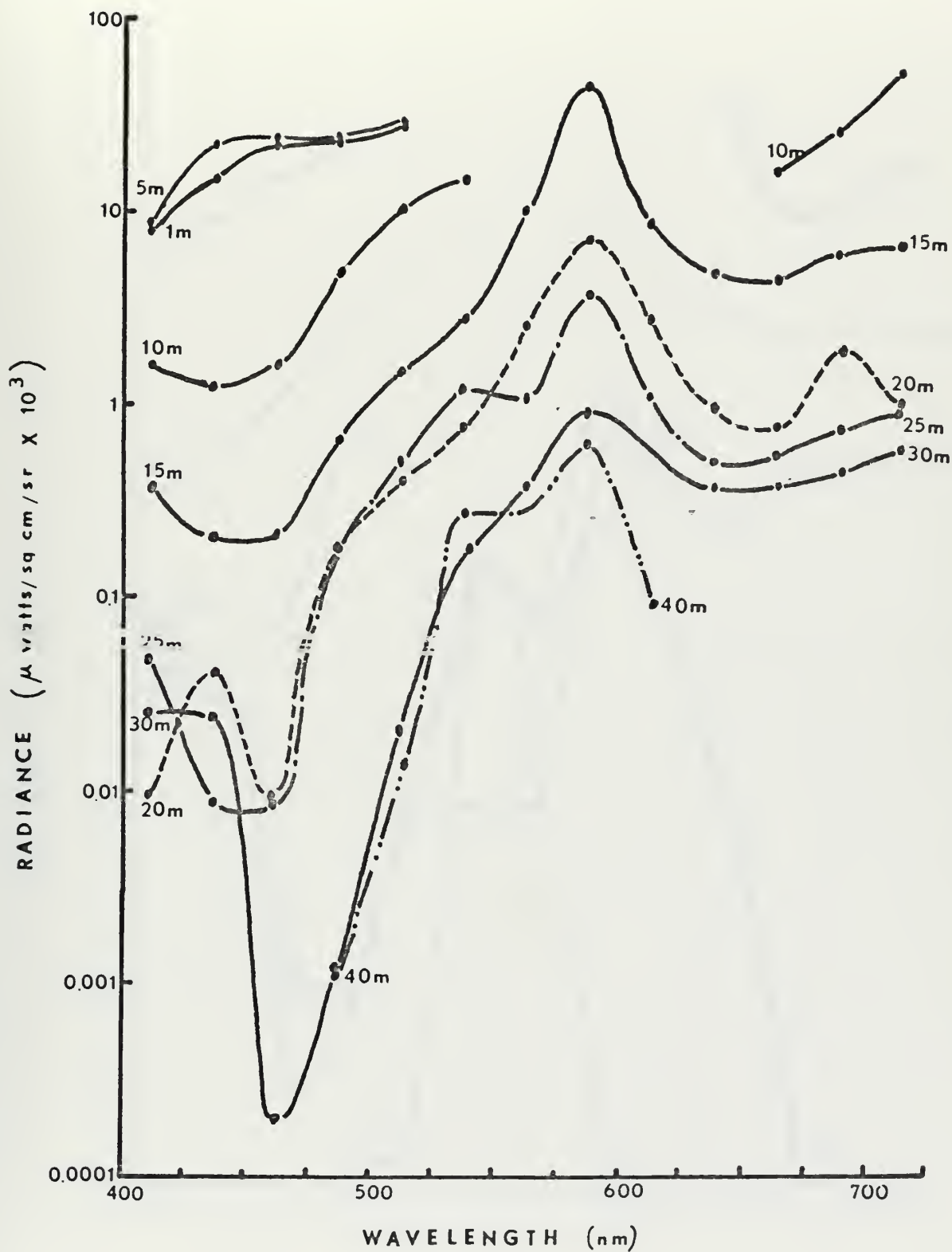


FIGURE 28. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\Theta = 45^\circ$ AND $\phi = 0^\circ$, STA 2.

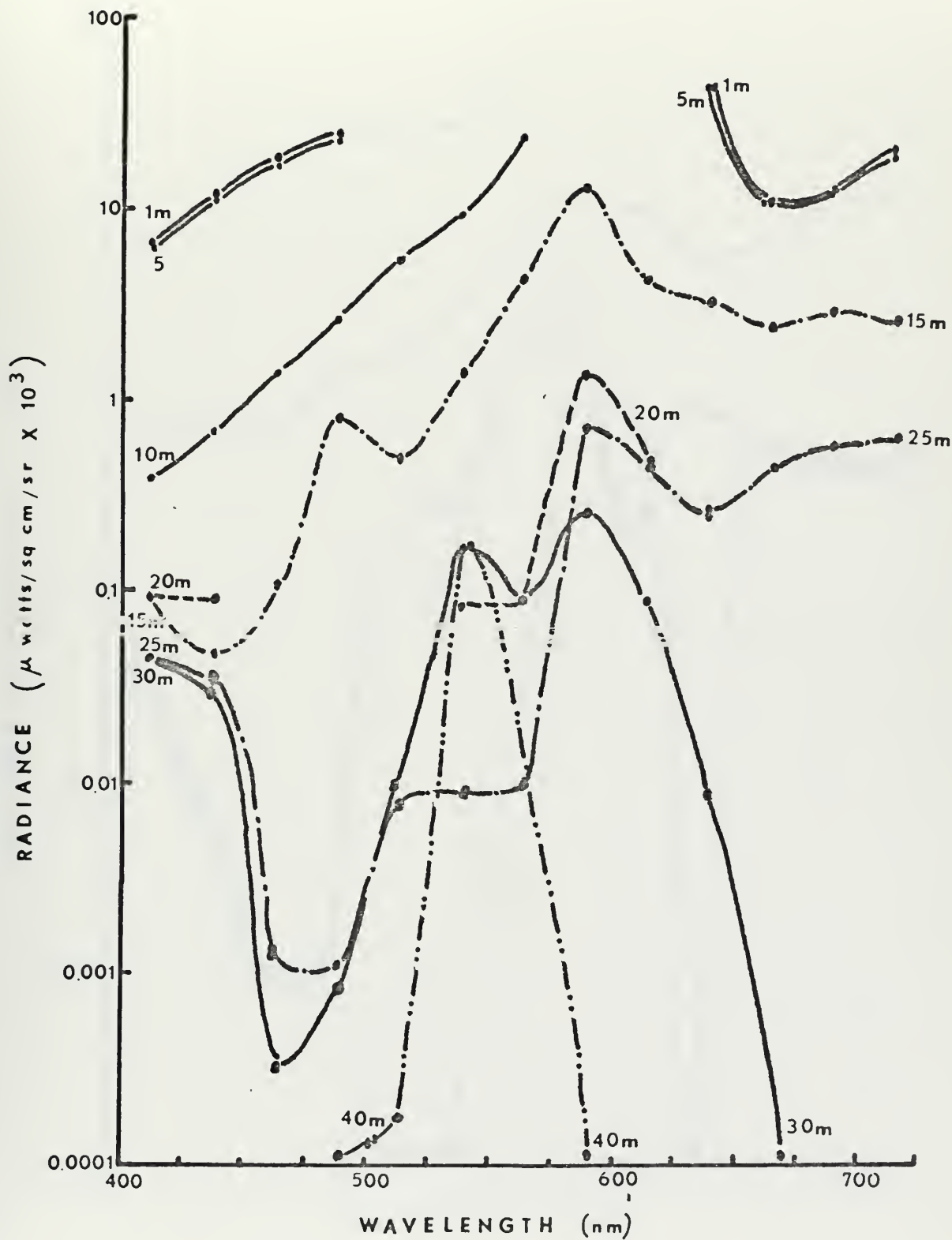


FIGURE 29. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\Theta = 90^\circ$ AND $\phi = 0^\circ$, STA 2

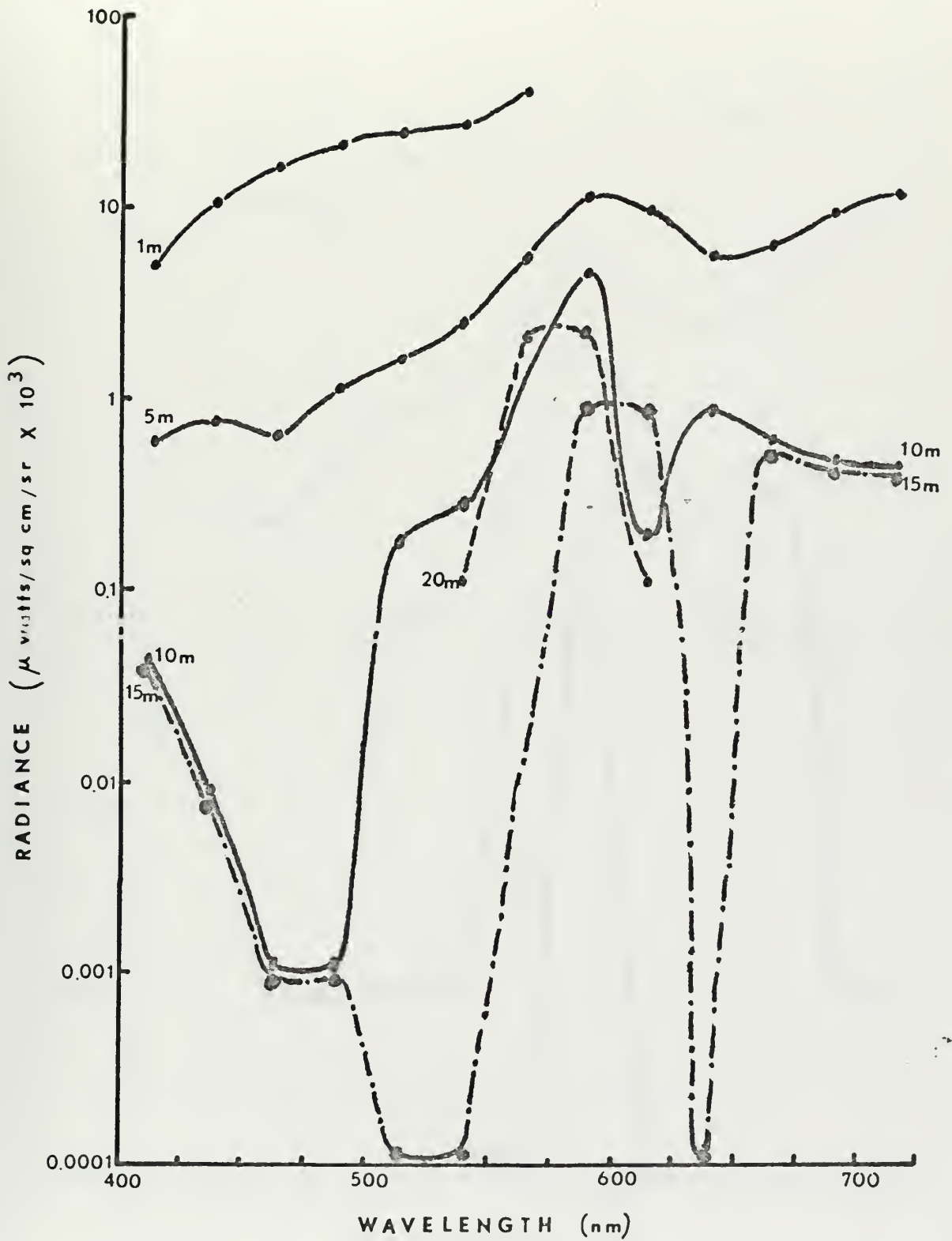


FIGURE 30. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\Theta = 135^\circ$ AND $\phi = 0^\circ$, STA 2

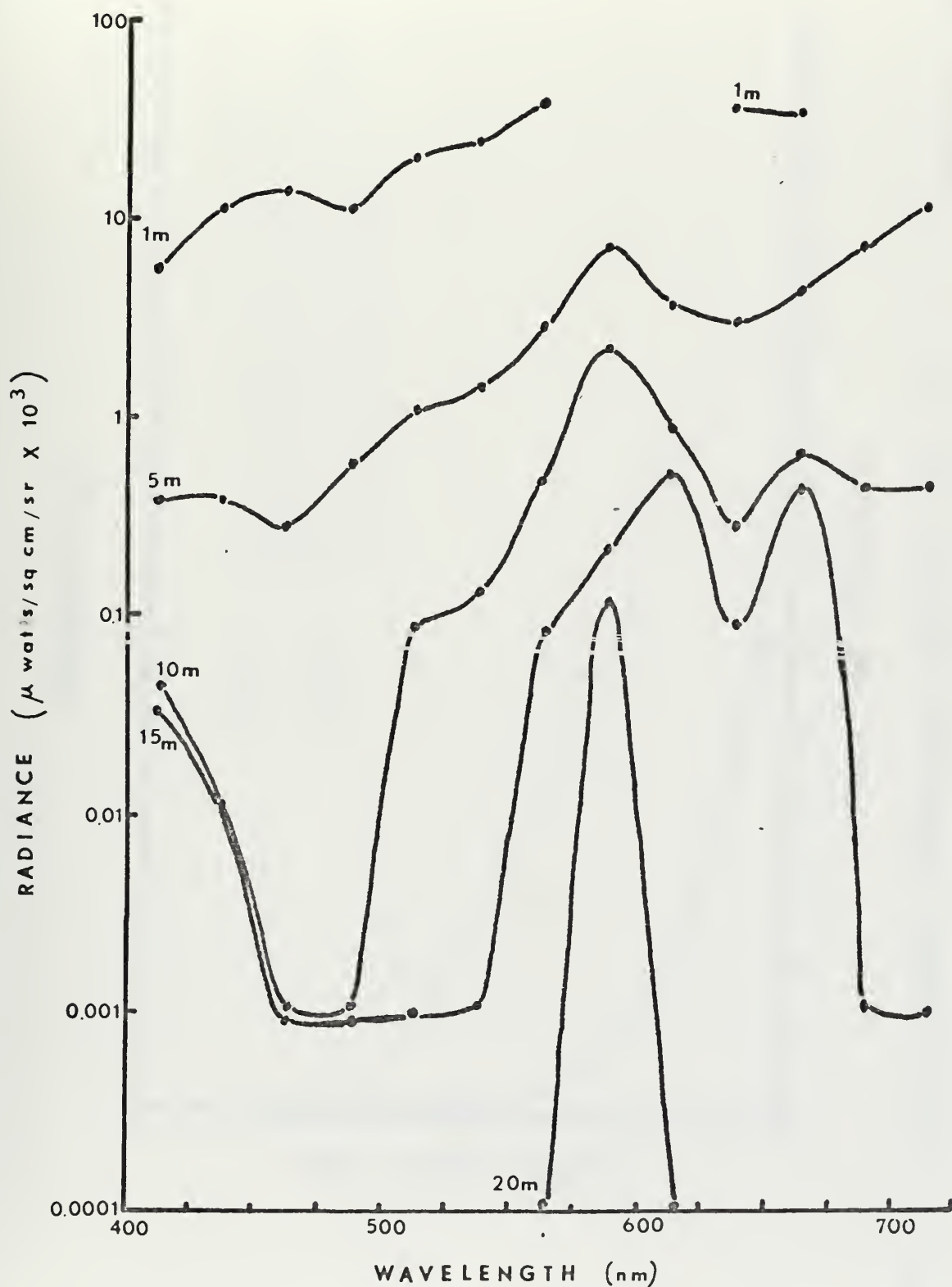


FIGURE 31. SPECTRAL RADIANCE DISTRIBUTION WITH DEPTH AT $\Theta = 166^\circ$ AND $\phi = 0^\circ$, STA 2

APPENDIX B

Spectral Radiance Calibration Nomograms for 25 nm Wavelength Bands from 400 to 725 nm.

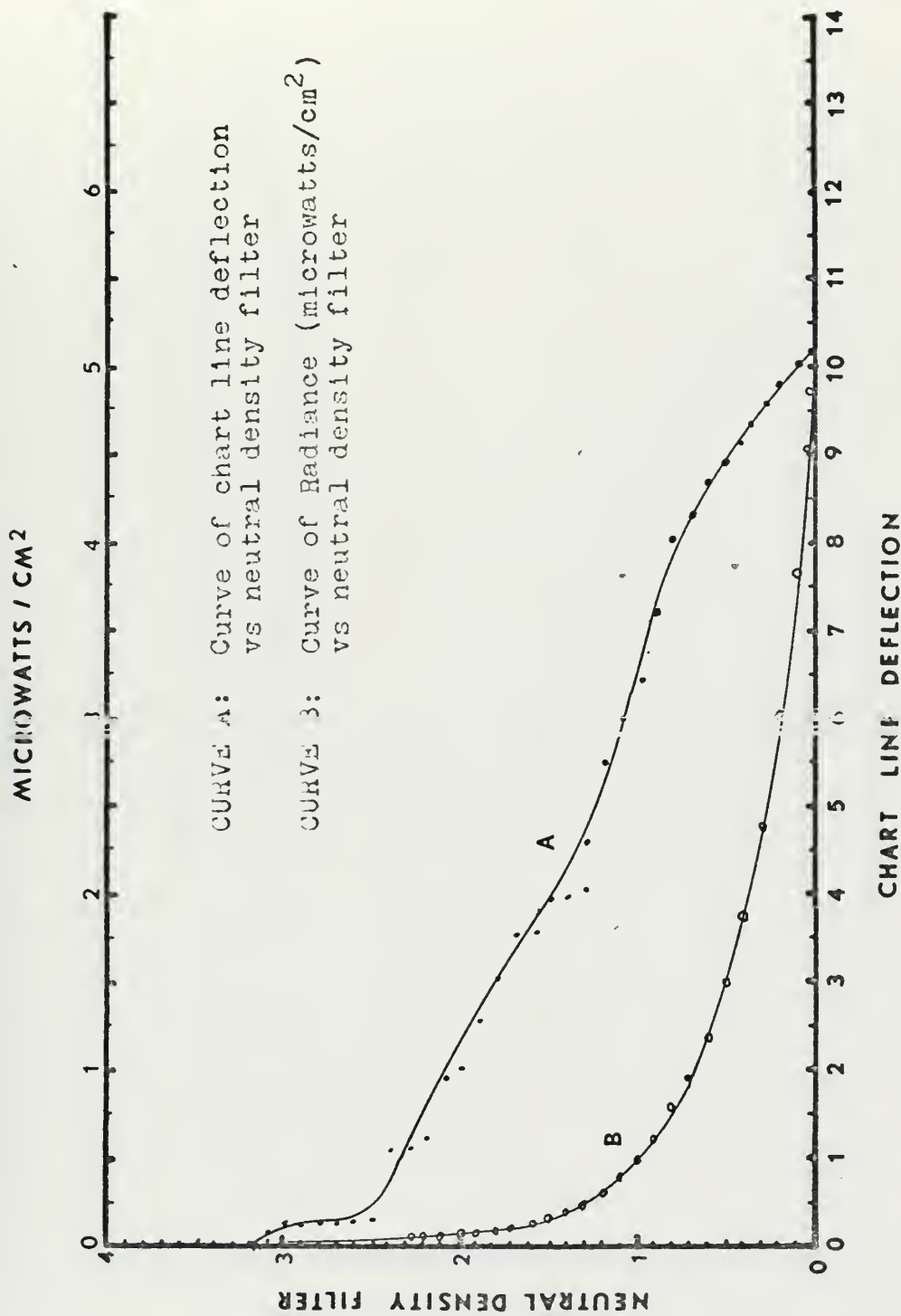


FIGURE 32. SPECTRAL RADIANCE CALIBRATION NOMOGRAM FOR 400 - 425 nm WAVELENGTH BAND

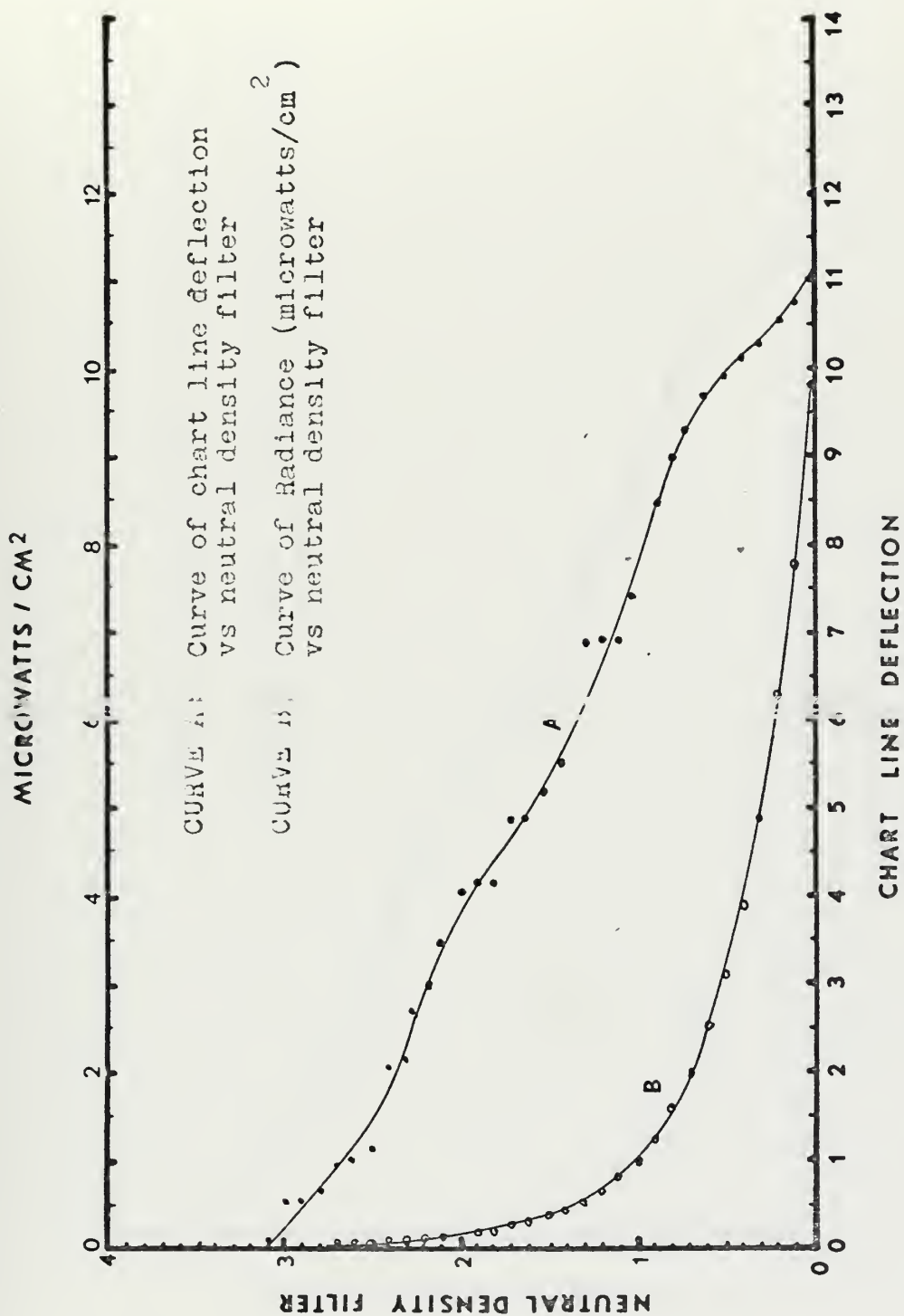


FIGURE 33. SPECTRAL RADIANCE CALIBRATION NEMOGRAM FOR 425-450 nm WAVELENGTH BAND .

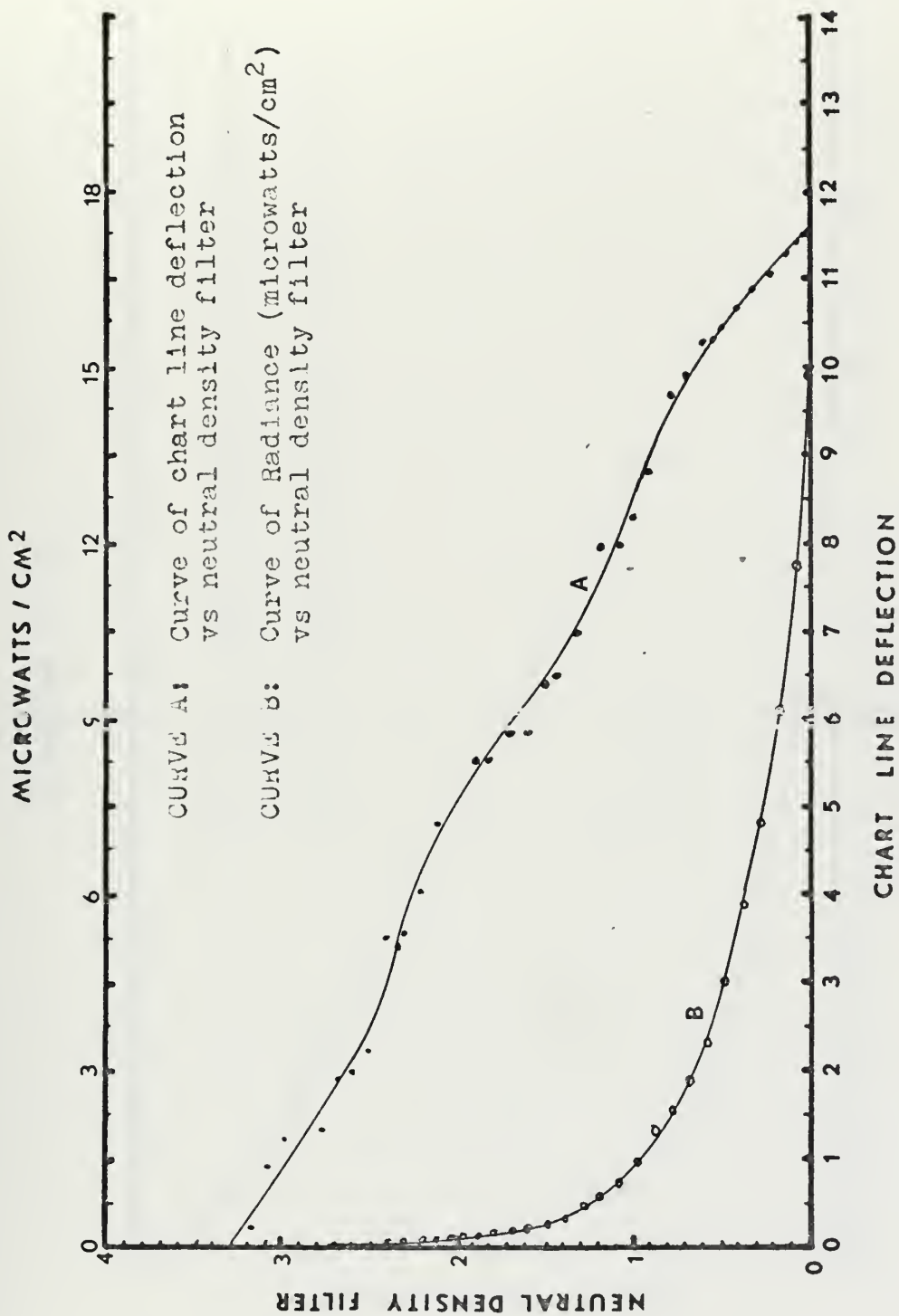


FIGURE 34. SPECTRAL RADIANCE CALIBRATION NIDMOGRAM FOR 450 - 475 nm WAVELENGTH BAND .

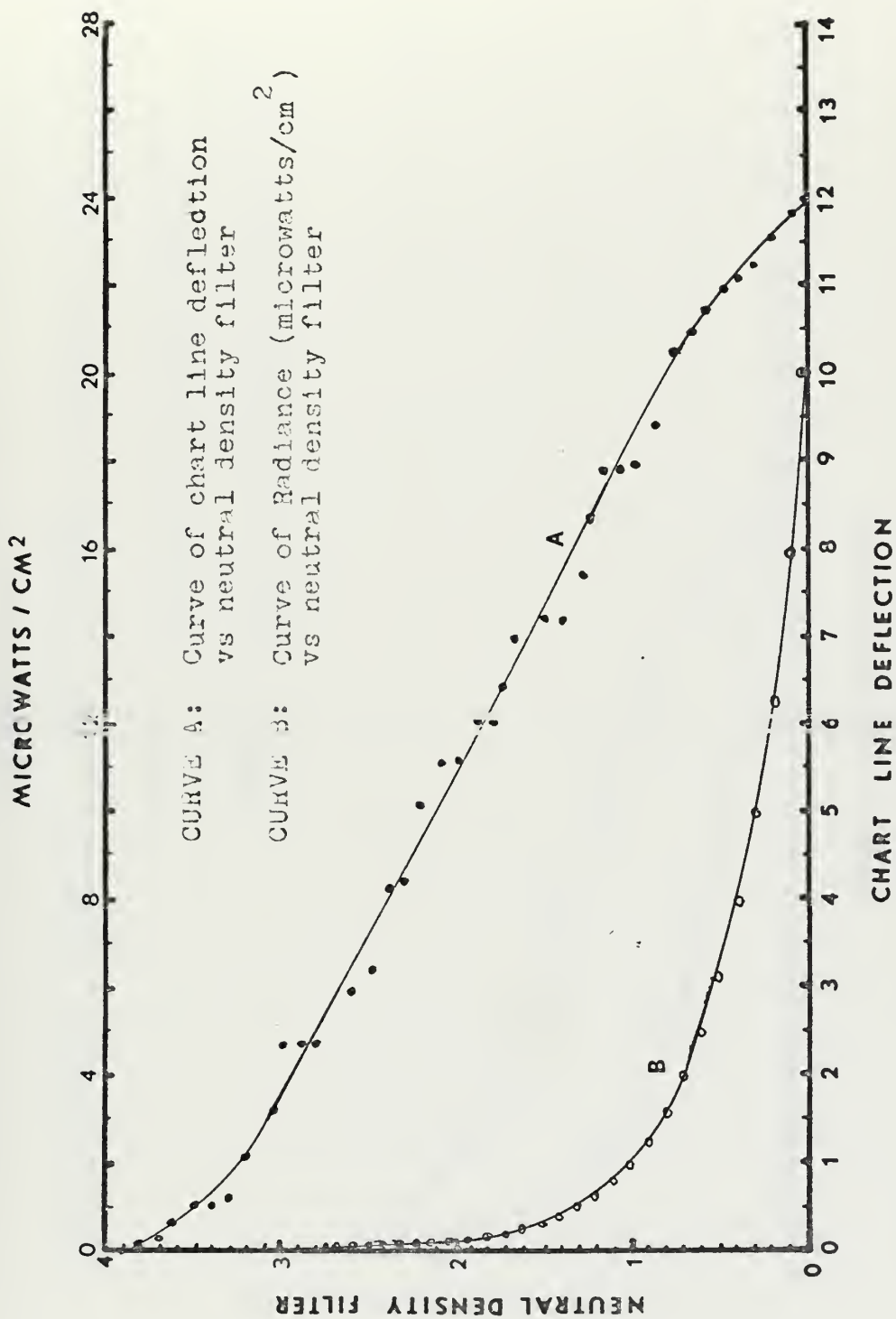


FIGURE 35. SPECTRAL RADIANCE CALIBRATION NOMOGRAM FOR 475-500 nm WAVELENGTH BAND

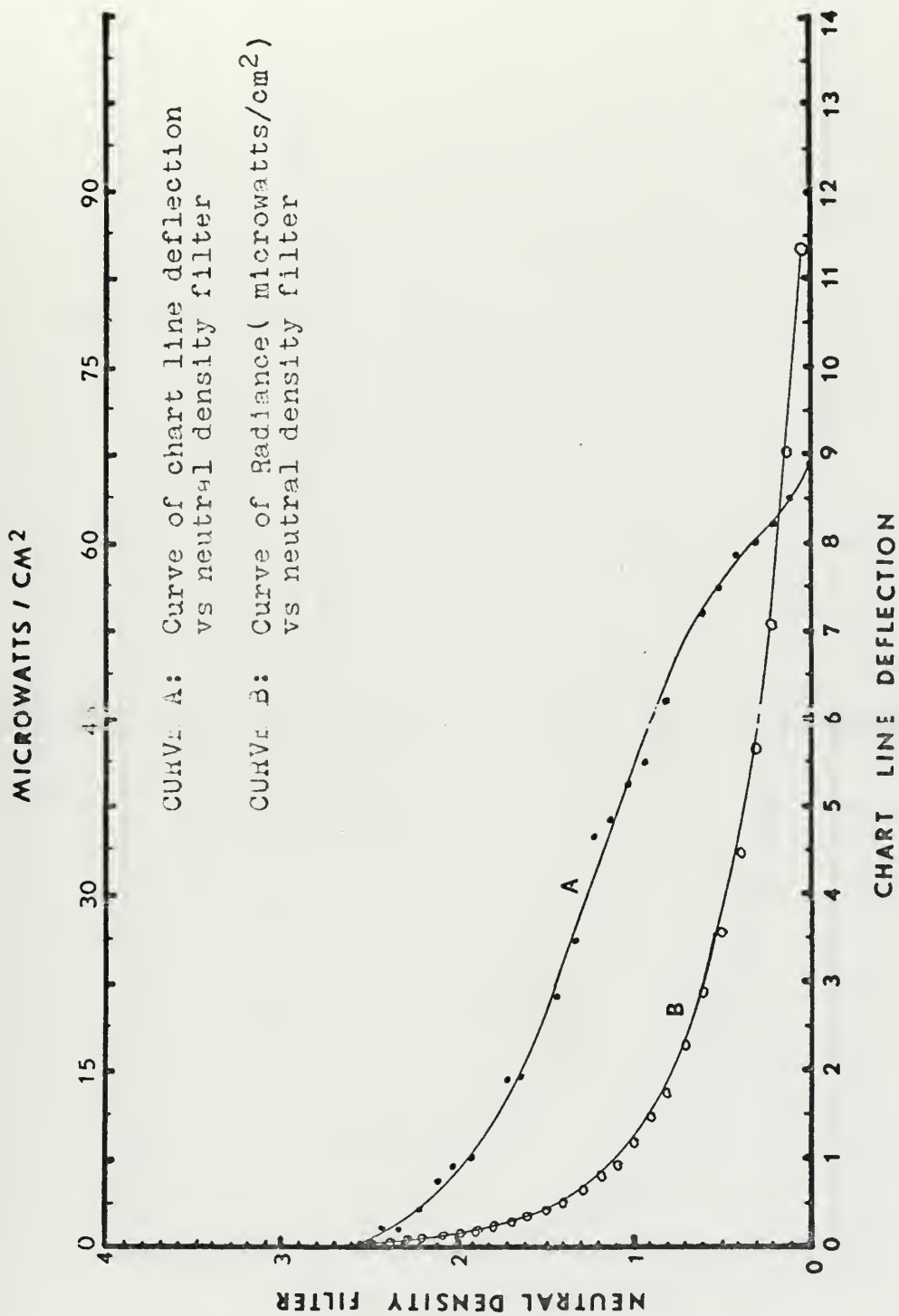


FIGURE 36. SPECTRAL RADIANCE CALIBRATION NOMOGRAM FOR 700-725 nm WAVELENGTH BAND

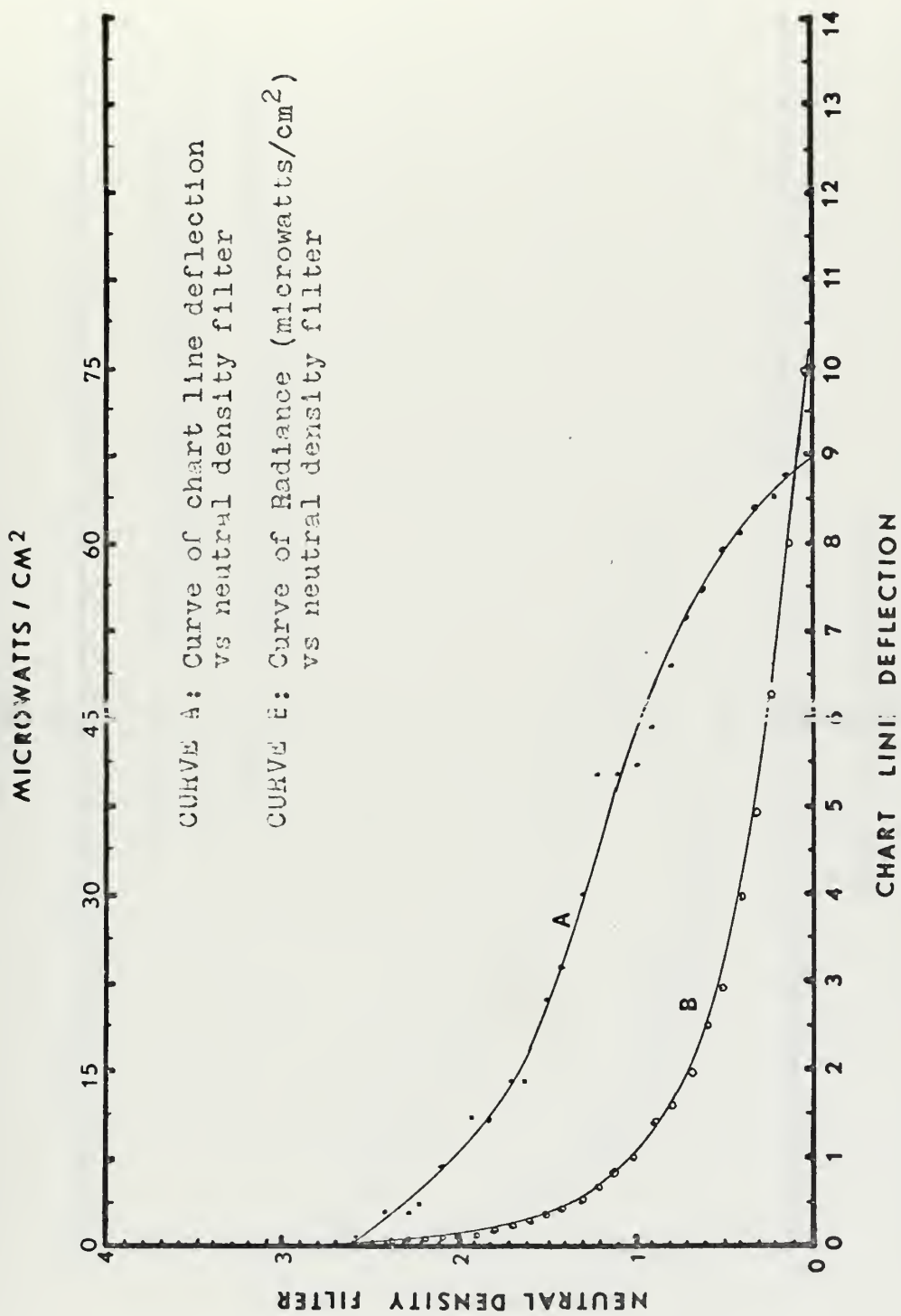


FIGURE 37. SPECTRAL RADIANCE CALIBRATION NOMOGRAM FOR 675-700 nm WAVELENGTH BAND

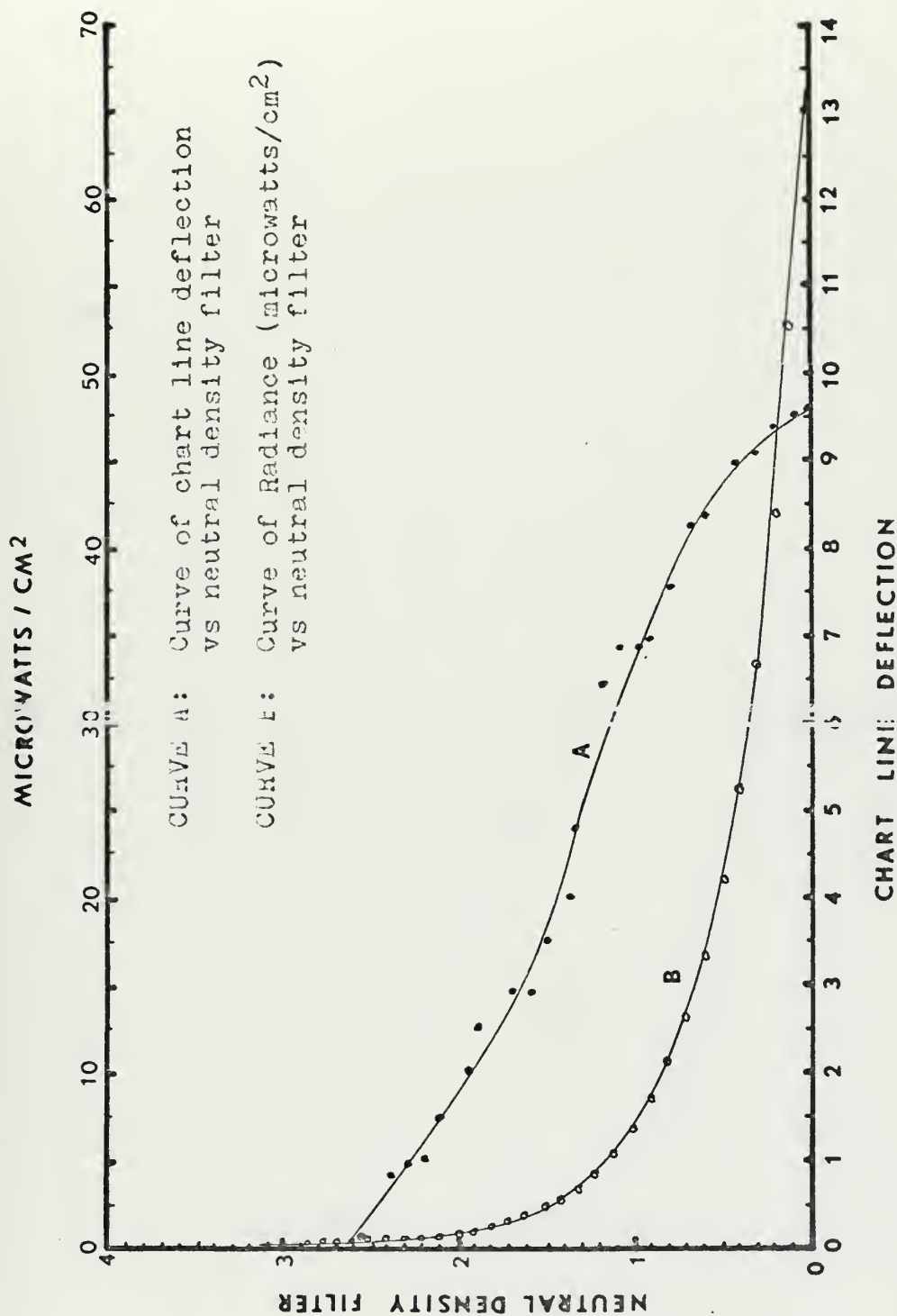


FIGURE 38. SPECTRAL RADIANCE CALIBRATION NOMOGRAM FOR 650-675 nm WAVELENGTH BAND

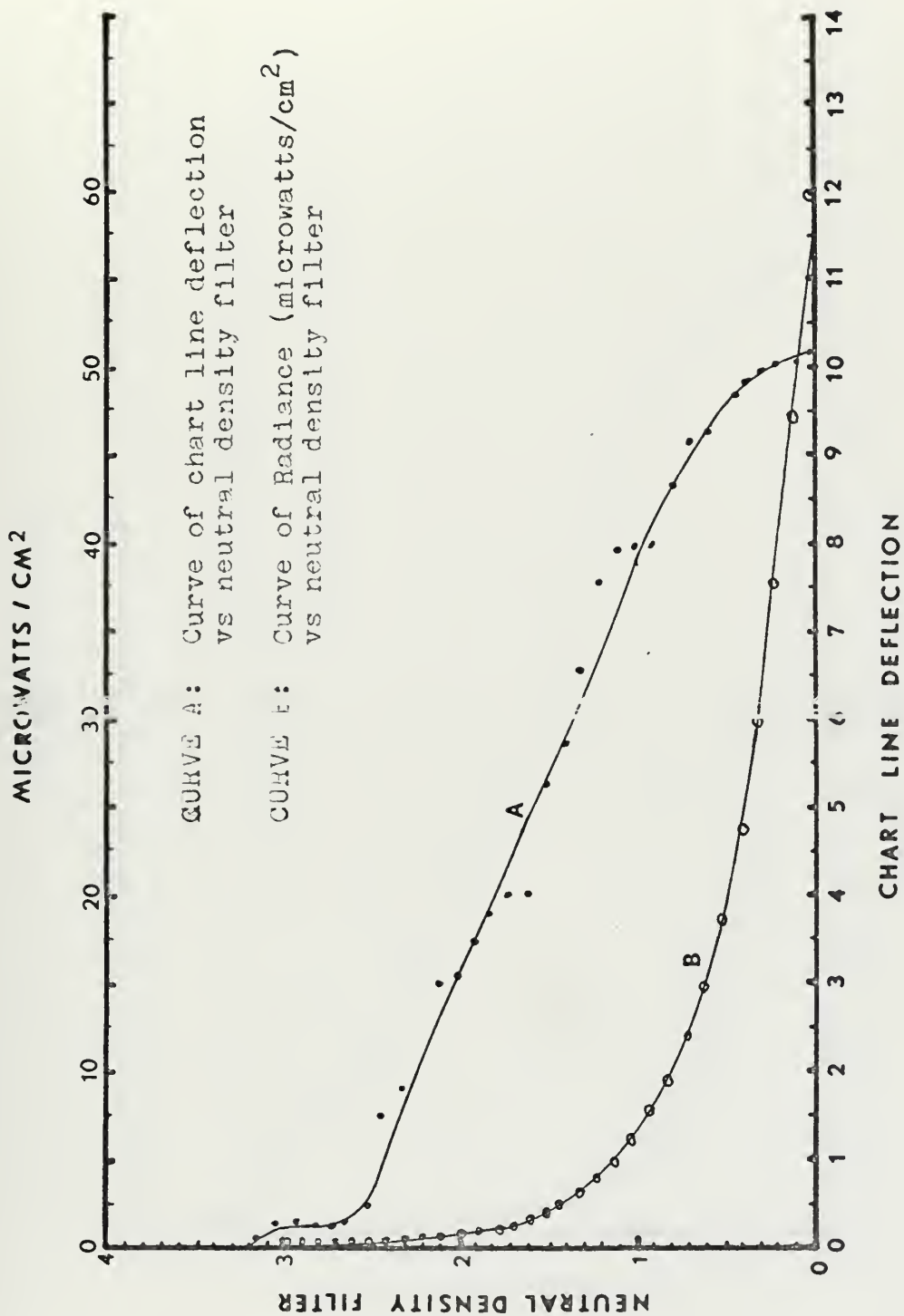


FIGURE 39. SPECTRAL RADIANCE CALIBRATION NCMOGRAM FOR 625 - 650 nm WAVELENGTH BAND .

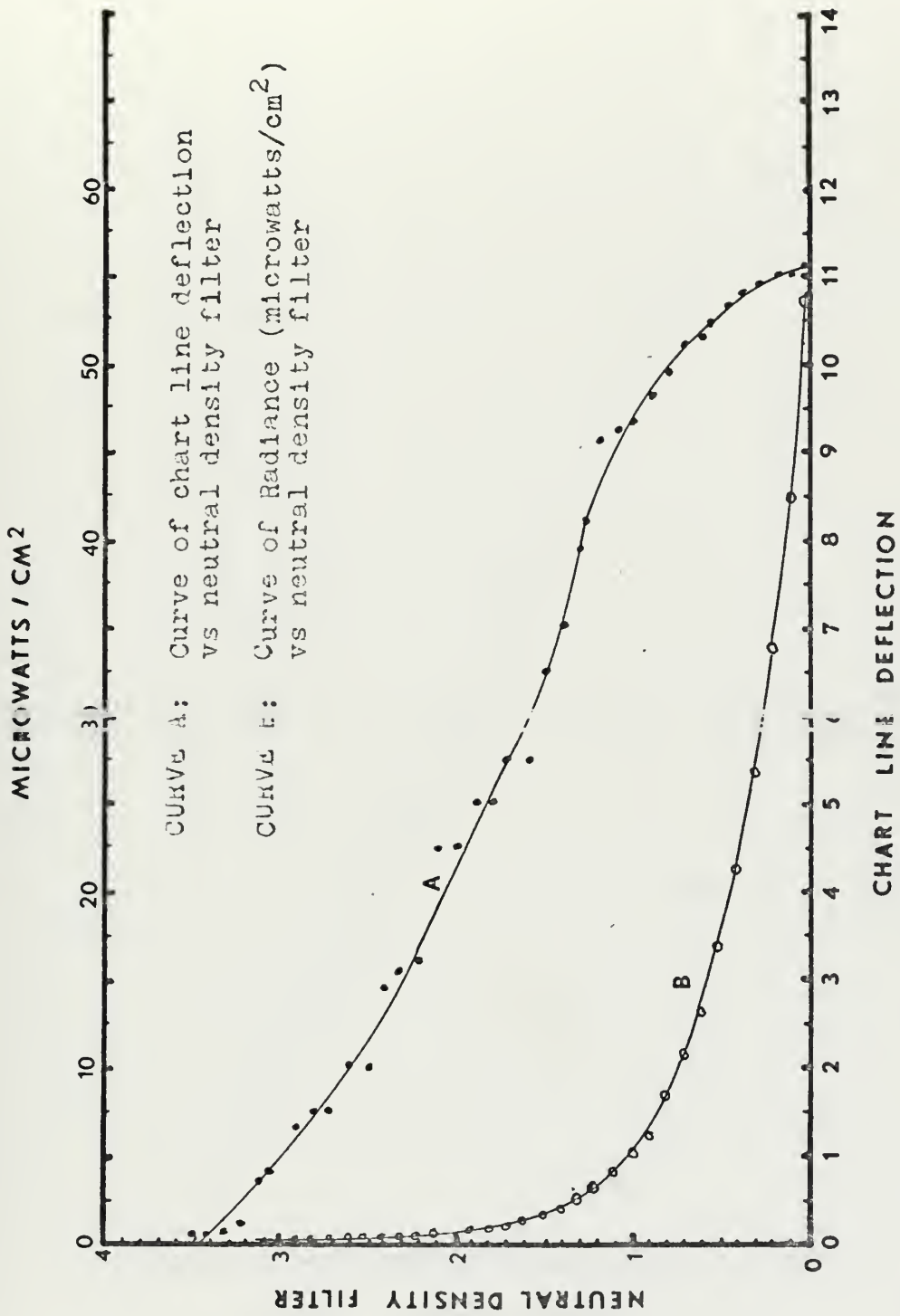


FIGURE 40. SPECTRAL RADIANCE CALIBRATION HOMOGRAM FOR 600-625 nm WAVELENGTH BAND

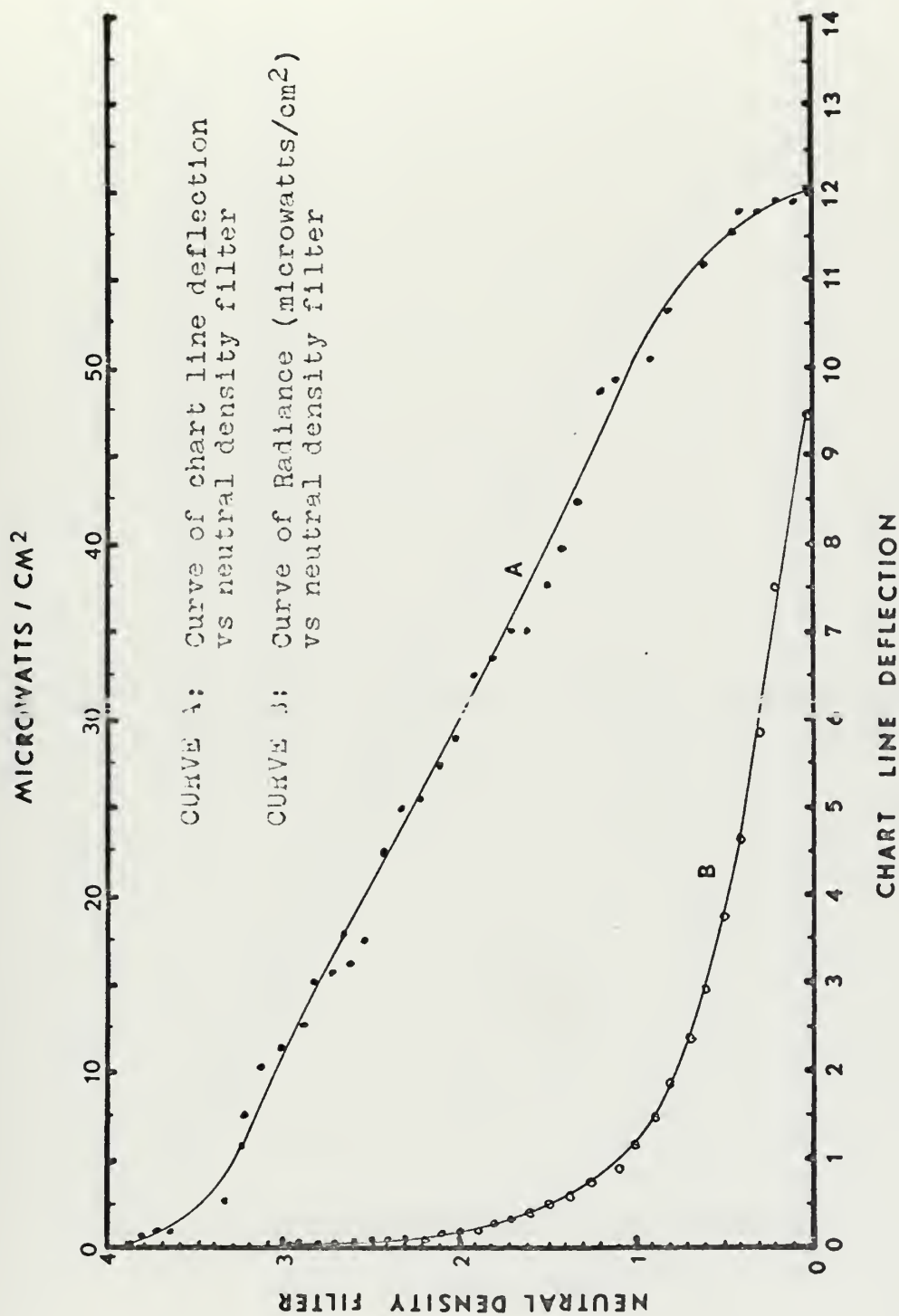


FIGURE 41. SPECTRAL RADIANCE CALIBRATION NCMOGRAM FOR 575 - 600 nm WAVELENGTH BAND .

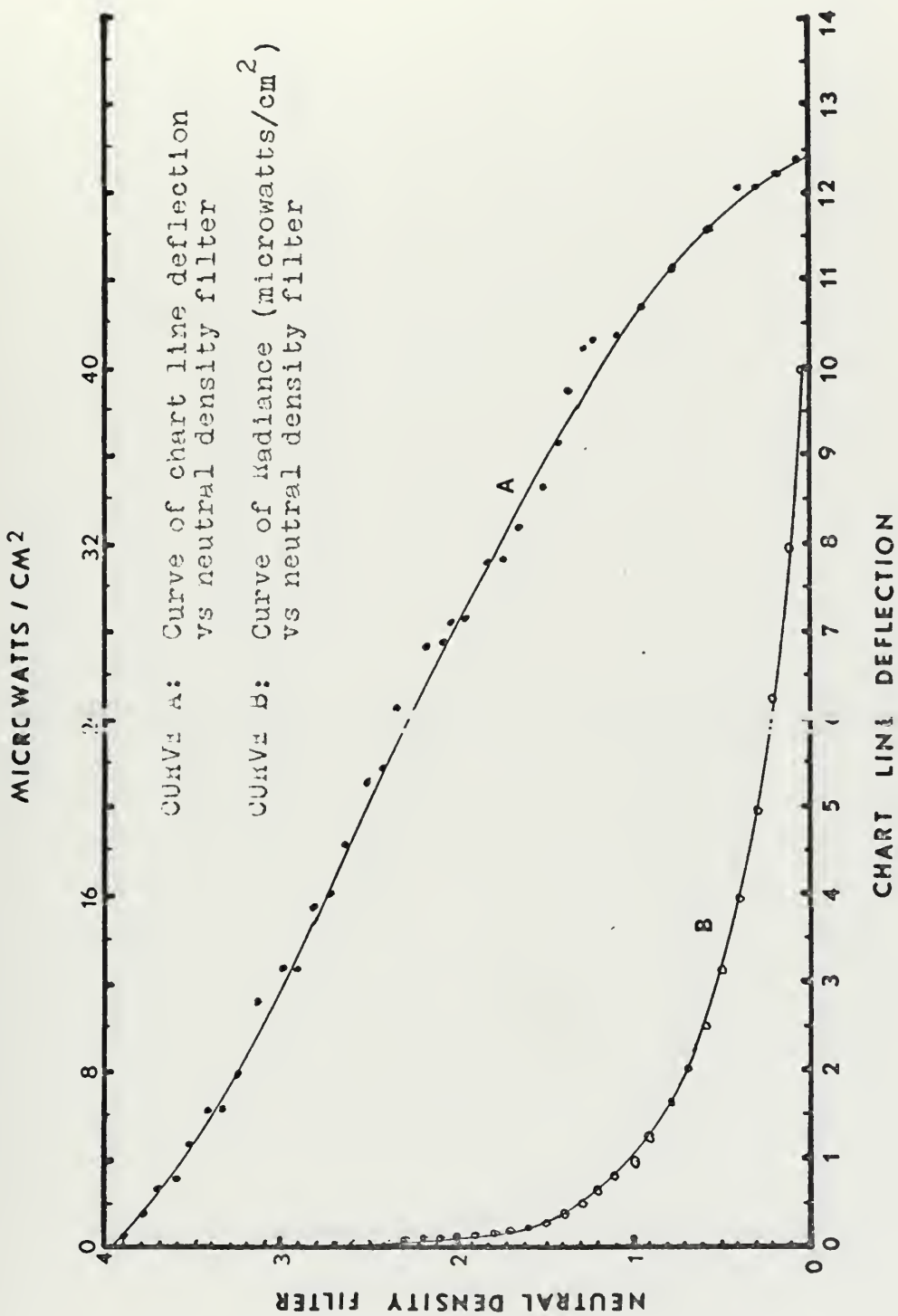


FIGURE 42. SPECTRAL RADIANCE CALIBRATION MONOGRAM FOR 550-575 nm WAVELENGTH BAND

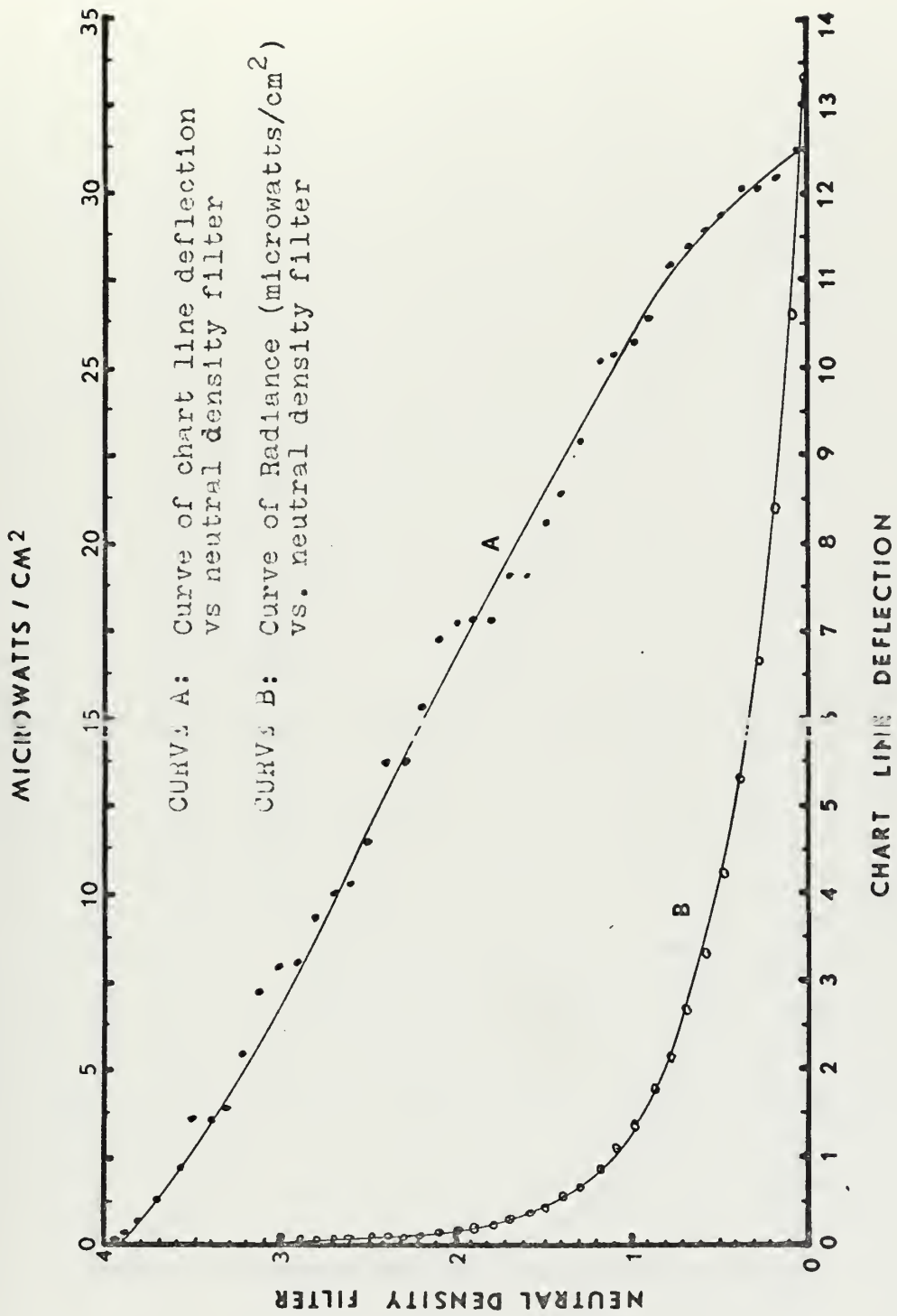


FIGURE 43. SPECTRAL RADIANCE CALIBRATION NOMOGRAM FOR 525-550 nm WAVELENGTH BAND

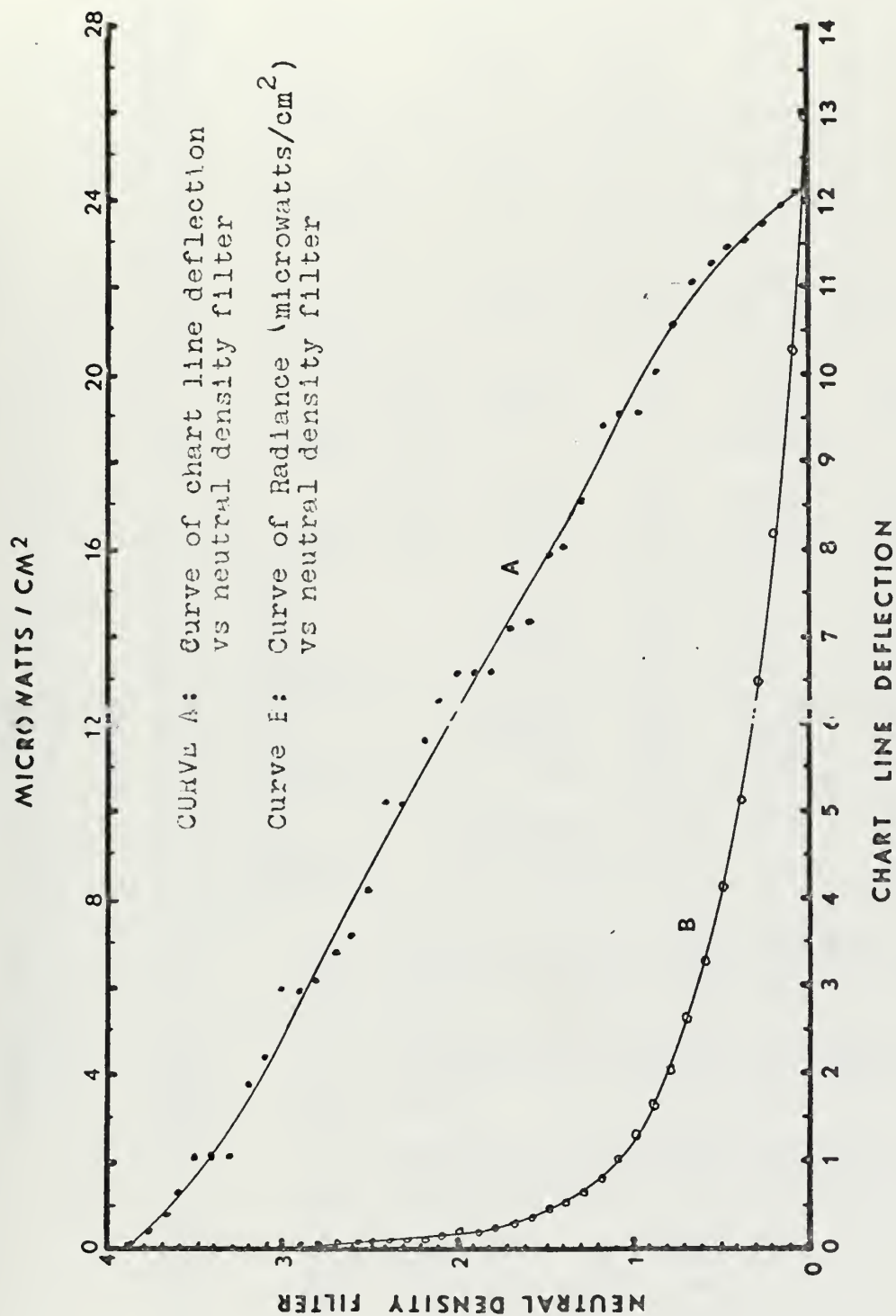


FIGURE 44. SPECTRAL RADIANCE CALIBRATION NEMOGRAM FOR 500 - 525 nm WAVELENGTH BAND

APPENDIX C

Station Data: Location, Date, Time, Depth, Weather, Altitude of the Sun, Azimuth of the Sun, Radiance Measurements.

Station 1

Latitude: 36-38.8 N Longitude: 121-52.6 W Date: 16 July 1971 Local Time: 1255-1325 Sea: 230-1/2
Swell: 260-2 Sky: Partially Overcast Average Altitude of the Sun: 69° Average Azimuth of the Sun: 180°T

Radiance ($\mu\text{W}/\text{cm}^2/\text{sr} \times 10^3$)

θ	Depth	φ	Wavelength Bands (nm)													
			400-425	425-450	450-475	475-500	500-525	525-550	550-575	575-600	600-625	625-650	650-675	675-700	700-725	
0°	10m	264	9.22	9.39	15.09	20.45	*	*	*	9.89	8.22	24.73	52.81	*	*	
		000	9.14	8.80	21.46	*	*	*	40.23	45.26	*	*	*	*		
		270	*	8.21	8.80	16.76	21.79	*	*	*	*	*	*	*		
	20m	130	5.45	0.59	.59	1.68	2.85	5.24	17.60	2.31	2.10	3.35	5.36	9.01	11.74	
		000	*	0.75	.67	1.68	2.85	5.24	17.60	5.03	2.51	3.35	4.61	6.71	9.47	
45°	10m	166	*	3.27	6.54	10.56	17.60	20.13	20.18	2.35	2.18	6.29	6.29	11.24	41.07	
		184	3.47	3.35	6.71	16.60	19.28	*	*	*	*	*	*	*		
		081	*	8.21	8.80	16.76	*	*	*	*	*	39.40	54.48	63.70	*	
		122	.50	.84	1.09	1.68	3.52	14.17	15.09	5.45	2.93	5.45	6.71	12.57	19.28	
		039	3.73	4.19	4.61	10.48	17.18	*	*	*	*	*	*	*	*	
		000	*	8.30	11.32	17.02	*	*	*	*	*	47.78	39.40	*	*	
		263	1.00	1.17	1.68	3.02	5.36	12.57	17.60	39.40	46.10	39.40	24.31	39.40	64.54	
		292	*	5.87	6.71	10.48	17.18	27.65	*	39.40	15.93	12.57	8.38	18.48	37.72	
		039	*	8.21	6.87	16.85	*	*	*	*	*	*	*	*	*	
		081	*	8.21	8.80	16.76	*	*	*	*	*	39.40	54.48	63.70	*	
		234	1.59	1.51	1.84	5.28	6.29	7.71	10.90	10.90	5.03	6.71	5.87	8.80	12.57	
		181	3.47	3.35	6.71	16.60	19.28	*	*	*	*	*	*	*	*	

θ	Depth	φ	400-	425-	450-	475-	500-	525-	550-	575-	600-	625-	650-	675-	700-	725-	700-
			234	8.21	8.21	15.09	21.46	*	*	5.03	5.45	15.51	5.45	*	*	*	
45°	20m	234	8.21	8.21	15.09	21.46	*	*	5.03	5.45	15.51	5.45	*	*	*		
		105	*	.17	.17	.34	.92	1.42	2.51	.84	.42	.63	1.34	2.10			
		309	*	.51	.59	1.01	1.51	2.26	1.20	1.05	.25	.08	.42	1.09			
		194	.17	.34	.42	1.01	1.84	4.19	1.36	2.93	2.10	1.68	1.68	2.51	3.19		
		341	2.93	5.03	.84	1.68	2.26	4.53	1.03	2.93	2.60	.84	3.35	3.77	4.61		
		000	2.51	.42	.42	1.01	2.26	5.87	6.71	6.87	2.93	1.26	3.35	6.29	9.64		

θ	Depth	φ	400- 425	425- 450	450- 475	475- 500	500- 525	525- 550	550- 575	575- 600	600- 625	625- 650	650- 675	675- 700	700- 725
90°	3m	000	4.15	3.94	4.36	6.71	9.22	8.47	13.41	12.74	10.48	37.72	18.02	45.26	69.15
		071	4.21	4.08	4.29	6.62	9.01	7.10	10.25	11.31	10.21	32.12	15.00	41.02	61.11
		142	3.95	3.50	4.21	6.43	8.68	5.02	5.11	8.99	10.11	40.01	41.28	50.85	*
		322	1.09	1.09	1.26	1.68	2.01	2.10	1.26	3.35	2.51	4.19	6.71	13.41	22.63
	5m	000	5.30	5.28	9.90	10.73	17.60	27.24	13.41	20.54	8.38	37.72	19.70	46.10	*
		020	3.89	3.55	4.35	5.02	7.91	9.53	8.03	8.81	5.11	5.85	9.52	20.10	48.31
		098	5.01	4.77	5.53	2.54	9.22	9.22	13.41	5.03	4.61	7.54	10.06	19.70	49.45
	7m	000	.89	1.34	1.43	2.35	4.55	5.24	8.74	5.02	3.77	5.41	10.00	15.71	22.78
		079	.85	1.30	1.40	2.28	4.29	5.15	8.65	5.05	3.60	5.29	9.90	14.85	21.65
	10m	033		.25	.17	1.01	1.34	1.59	2.51	1.26	1.04	1.05	3.35	5.20	6.71
		176		.25	.17	.84	1.34	1.68	2.51	2.10	1.26	1.04	2.72	5.11	6.71
		163	.08	.25	.008	.42	.84	1.68	1.17	2.10	1.68	.84	.84	1.68	2.51
		078	.21	.34	.42	.84	2.51	4.19	4.19	3.77	2.10	2.10	3.35	5.87	7.12
		000	.46	.92	1.26	2.18	2.51	5.03	6.54	11.74	14.67	4.61	3.35	6.29	10.06
		297	.38	.84	.50	1.21	2.51	4.61	5.36	7.12	2.93	4.61	3.35	6.29	10.06
		329	.50	.75	.75	.84	2.51	10.48	5.36	7.12	2.51	4.61	2.51	5.45	6.71
		111	1.01	1.17	1.27	1.68	1.68	3.19	5.05	10.48	2.10	2.93	3.35	6.29	10.06
		260	.25	.42	.34	.42	.84	1.59	2.68	5.45	2.51	1.26	2.51	3.77	5.03
	20m	000	0	.001	.01	.17	.17	.25	.42	.001	.001	.001	.001	.001	0
		167	0	.08	.08	.17	.34	.34	.34	.42	.001	.001	.001	.0001	0
		294	.042	.042	.008	.25	.586	.84	1.68	1.68	.84	.42	.17	.42	.008
		067	.50	.042	.017	.251	.42	.84	.84	1.93	.84	.42	.34	.42	.008
		137	.001	.001	.008	.167	.167	.420	.670	.84	.67	.34	.47	.42	.34
		104	.001	.001	.008	.13	.17	.34	.42	1.26	.50	.50	.42	.59	.34
		000	.008	.050	.017	.34	.84	1.26	1.26	.84	2.10	.84	.50	.67	.50

θ	Depth	φ	400-	425-	450-	475-	500-	525-	550-	575-	600-	625-	650-	675-	700-
			425	450	475	500	525	550	575	600	625	650	675	700	725
135°	3m	000	.92	2.15	2.52	9.21	5.01	6.00	1.28	8.61	6.14	6.34	10.14	13.38	30.15
		334	.85	1.34	1.68	2.35	3.19	3.02	.26	3.35	3.35	6.29	9.22	11.24	22.63
		251	.922	.922	.922	.922	2.01	2.01	1.60	3.35	2.93	5.45	9.72	16.55	26.82
	5m	000	.922	.922	.922	.922	2.01	2.18	1.60	3.35	2.93	5.45	9.72	16.55	26.82
		000	1.27	1.29	1.15	2.31	3.51	3.65	1.81	5.28	4.25	4.03	3.54	1.10	1.19
	10m	143	.82	.84	.75	.84		1.05	1.47	2.18	2.51	5.45	9.22	15.51	22.63
		122	.04	.08	.08	.34	.84	.42	.59	.08	.001	.001	.001	.84	.84
		340	.04	.08	.08	.16	.42	.38	.59	.08	.001	.001	.001	.84	.84
		098	.04	.08	.08	.17	.34	.50	.67	1.67	1.51	1.09	.84	.84	.84
		303	.04	.08	.17	.25	.34	.50	1.01	2.10	1.26	.34	.84	1.67	2.51
		340	.05	.08	.08	.25	.34	.50	.84	1.68	1.26	.34	.34	.84	.84
		000	.08	.08	.17	.25	.42	2.10	2.10	2.51	1.68	1.26	.34	2.10	1.68
		137	.59	.08	.08	.25	.34	.50	1.01	2.51	2.10	1.26	.92	2.10	2.51
20m	341	.0006	.001	.001	.001	.001	.001	.21	.08	.001	.001	.001	.001	.001	0
	118	.0007	.001	.001	.001	.08	.21	.08	.001	.001	.001	.001	.001	.001	0
	176	.0008	.008	.008	.008	.012	.251	.08	.17	.008	.17	.08	.59	.008	.008
	120	.0008	.008	.008	.008	.042	.251	.083	.008	.008	.34	.17	.59	.008	.008
	000	.042	.008	.0008	.008	.017	.251	.084	.034	.503	.251	.084	.419	.008	.008
	3m	000	1.71	1.73	2.19	2.87	3.68	4.19	4.93	5.21	3.89	4.51	4.72	17.29	25.18
		120	1.60	1.51	1.93	2.85	3.02	3.86	2.51	3.77	2.93	5.45	19.11	16.76	22.63
	5m	209	.93	.92	.75	1.34	1.34	1.51	.75	2.18	2.10	4.19	6.37	10.48	14.25
000		.99	1.01	1.26	2.01	1.84	2.31	4.02	3.35	2.51	5.45	12.57	16.76	25.15	
7m	314	.90	.92	.92	2.01	1.84	3.86	2.43	3.77	2.93	5.45	12.57	16.76	25.15	
	000	.65	.75	.59	.67	1.17	1.26	1.68	2.93	2.51	5.45	4.80	3.83	1.97	
10m	136	.59	.75	.59	.82	1.01	1.26	1.68	2.10	2.51	5.45	4.80	3.83	1.97	
	232	.04	.08	.08	.08	.17	.21	.82	.34	.34	.001	.82	1.01	1.68	
	244	.04	.08	.08	.08	.17	.21	.82	.82	.34	.001	.41	.82	2.10	
	201	.042	.06	.008	.17	.42	.50	.50	1.26	.84	.42	.42	1.01	1.68	
	021	.05	.08	.008	.17	.37	.67	.84	1.68	.92	.59	.50	.92	1.68	

*Values exceed limitations of standard lamp

Station 2

Latitude: 36-39.7 N Longitude: 121-53.7 W Date: 16 July 1971 Local Sun Time 1410-1440
 Sea: 230-1/2. Swell: 230-2. Sky: Overcast. Average Altitude of the Sun: 65°. Average Azimuth
 of the Sun: 230°T

Radiance ($\mu\text{w}/\text{cm}^2/\text{sr} \times 10^3$)

Wavelength Bands (nm)

θ	Depth	φ	Wavelength Bands (nm)															
			400- 425	425- 450	450- 475	475- 500	500- 525	525- 550	550- 575	575- 600	600- 625	625- 650	650- 675	675- 700	700- 725	725- 750	750- 775	775- 800
0°	5m	000	5.12	10.98	16.51	23.30	23.64	*	*	*	*	*	*	*	*	*	*	*
		298	5.00	10.88	16.43	23.10	22.64	*	*	*	*	*	*	*	*	*	*	*
	10m	000	.67	.84	1.17	2.93	9.22	14.00	*	*	*	39.40	19.70	44.30	69.20			
		050	1.09	.92	1.34	4.27	7.04	5.64	33.53	*	*	10.51	7.52	11.74	15.30			
15m	235	.34	.17	.17	.17	.50	1.34	2.18	10.06	24.31	8.38	2.10	2.10	3.35	5.03			
		.17	.17	.17	.17	.34	1.34	1.51	10.06	39.40	8.38	5.03	4.19	4.19	5.45			
	000	.17	.17	.17	.17	.34	1.34	1.51	10.06	39.40	8.38	5.03	4.19	4.19	5.45			
		.21	.42	.25	.17	1.68	2.35	7.71	10.56	4.19	2.68	3.35	3.35	5.03	6.29			
20m	185	.08	.25	.17	.17	1.01	1.76	4.61	15.09	4.19	2.68	5.45	5.45	6.29	9.64			
		.08	.04	.04	.04	.17	.34	.67	2.10	8.21	2.35	1.26	2.10	1.68	2.51			
	000	.08	.059	.059	.034	.168	.335	.838	1.005	2.515	.838	.251	.419	.671	.671			
		.075	.008	.008	.025	.042	.754	2.096	1.676	1.676	.503	.251	.335	.419	.419			
25m	024	.034	.008	.008	.084	.335	1.090	2.514	1.676	2.096	.838	.419	.419	.503	.587			
		.050	.008	.008	.001	.083	.17	.29	.50	1.09	0.84	0.42	0.42	0	0			
	30m	.04	.01	.01	.001	.042	.17	.29	.84	1.86	1.26	.42	.42	0	0			
		.008	.008	.008	.034	.042	.17	.34	.84	1.26	.34	.42	.167	0	0			
30m	032	.008	.008	.008	.034	.042	.17	.34	.84	1.26	.34	.42	.167	0	0			
		.008	.001	.0008	.0008	.042	.084	.251	1.676	.419	.335	.017	.419	.167	.419			
	188	.008	.008	.008	.034	.042	.17	.29	.84	1.86	1.26	.42	.42	0	0			
		.008	.008	.008	.034	.042	.17	.34	.84	1.26	.34	.42	1.67	0	0			
30m	032	.008	.008	.008	.034	.042	.17	.34	.84	1.26	.34	.42	1.67	0	0			
		.008	.001	.0008	.0008	.042	.084	.251	.838	.671	.251	.017	.419	0	0			
	136	.0008	.001	.0008	.0008	.084	.167	1.257	1.005	1.676	.838	.335	.419	.167	.419			
		.017	.017	.0008	.0008	.084	.167	1.257	1.005	1.676	.838	.335	.419	.167	.419			
30m	070	.025	.034	.008	.008	.042	.008	1.676	1.005	.419	.335	.335	.419	.167	.335			
		.025	.034	.008	.008	.042	.008	1.676	1.005	.419	.335	.335	.419	.167	.335			
	070	.025	.034	.008	.008	.042	.008	1.676	1.005	.419	.335	.335	.419	.167	.335			
		.025	.034	.008	.008	.042	.008	1.676	1.005	.419	.335	.335	.419	.167	.335			

θ	Depth	φ	400- 425	425- 450	450- 475	475- 500	500- 525	525- 550	550- 575	575- 600	600- 625	625- 650	650- 675	675- 700	700- 725
40m	287	0	0	0	0	0	.083	.251	.628	.42	.251	.083	0	0	0
	127	0	0	0	0	0	.083	.251	.628	.42	.083	.083	0	0	0
	149	.0008	.001	.042	.168	.168	.168	.838	.251	.838	.251	.083	.419	.0008	.084
	000	.034	.042	.017	.083	.083	.168	.502	.87	.838	.168	.050	.419	.008	.084
	077	.034	.838	.0008	.042	.083	.042	.419	.03	.671	.251	.050	.419	.0008	.084
50m	194	.042	.017	.838	.042	.042	.042	.419	.419	2.096	.838	.083	.419	.084	.084
	241	0	0	0	0	0	0	.083	.167	.167	0	0	0	0	0
	209	0	0	0	0	0	0	.083	.095	.167	0	0	0	0	0
	111	0	0	0	0	0	0	.083	.083	.251	0	0	0	0	0
	032	.042	.017	.0008	.017	.008	.008	.419	.68	.671	.838	.042	.008	.008	.083
60m	000	.042	.001	.0008	.042	.042	.042	.419	.68	.838	.251	.419	.419	.083	.419
	205	.034	.017	.0008	.083	.419	.419	.419	.168	.754	.335	.419	.419	.083	.503
	041	0	0	0	0	0	0	.083	0	0	0	0	0	0	0
	260	0	0	0	0	0	0	.083	0	0	0	0	0	0	0
	231	.0008	0	0	.008	.017	.168	.168	.042	.042	.008	0	0	0	0
45° 1m	000	.017	0	0	.042	.042	.084	.168	.042	.042	.008	.084	0	0	0
	150	.008	0	0	.008	.0008	.0008	.168	.034	.042	.004	.167	0	0	0
	334	6.62	13.33	19.36	25.31	*	*	*	*	*	*	*	*	*	*
	039	5.53	11.06	16.76	22.63	*	*	*	*	*	*	*	*	*	*
	000	6.28	12.41	18.78	24.81	*	*	*	*	*	*	*	*	*	*
5m	263	5.78	16.42	18.69	24.81	*	*	*	*	*	*	*	*	*	*
	217	6.20	16.66	18.69	24.48	*	*	*	*	*	*	*	*	*	*
	000	6.45	17.95	18.74	24.81	*	*	*	*	*	*	*	*	*	*
	303	5.45	10.81	16.35	22.46	*	*	*	*	*	*	*	*	*	*
	176	5.78	11.65	17.60	24.31	*	*	*	*	*	*	*	*	*	*
	149	5.88	11.82	17.17	24.31	*	*	*	*	*	*	*	*	*	*
	025	4.86	9.64	15.09	20.96	20.12	*	*	*	*	*	*	*	*	*

θ	Depth	φ	400- 425	425- 450	450- 475	475- 500	500- 525	525- 550	550- 575	575- 600	600- 625	625- 650	650- 675	675- 700	700- 725
45°	10m	026	.34	.25	.17	.84	1.34	2.18	8.55	37.22	38.56	8.38	6.71	11.32	18.86
		000	1.51	1.17	1.51	3.77	8.55	12.74	*	*	*	*	15.51	23.47	44.41
		045	.34	.34	.25	1.01	1.93	5.28	17.60	*	*	15.51	7.96	11.32	20.96
		072	.75	1.01	1.26	3.02	6.20	8.23	*	*	*	15.51	10.06	12.57	20.96
		201	.083	.042	.017	.335	.42	1.09	3.44	19.28	3.77	5.45	3.77	5.28	5.87
15m		227	.083	.083	.17	.59	1.51	2.18	5.62	3.21	8.38	4.19	3.77	5.03	5.87
		331	.13	.13	.17	.59	.92	2.18	8.47	32.10	5.45	4.19	3.77	5.45	5.87
		000	.34	.17	.17	.59	1.26	2.18	8.47	39.61	7.12	4.19	3.77	5.45	5.45
		301	.168	.251	.083	.671	3.856	7.711	17.602	18.860	2.682	2.515	3.352	5.029	6.287
		159	.117	.335	.251	1.005	2.347	7.711	10.897	6.873	2.682	2.933	2.096	2.515	2.934
20m		340	.008	.01	.001	.01	.17	.34	.82	2.31	.82	.41	0	0	0
		000	.008	.042	.008	.17	.34	.63	2.10	6.54	2.51	.82	.63	1.68	.82
		085	.025	.042	.008	.168	.168	1.675	2.515	2.933	.838	.419	.419	.670	1.02
		290	.042	.008	.001	.001	.001	.003	.251	.63	2.93	.92	.42	0	0
		111	.034	0	0	0	0	.03	.167	.251	.042	.01	0	0	0
25m		101	.034	0	0	0	0	.03	.08	.63	.042	.08	0	0	0
		044	.059	.059	.013	.008	.335	.833	.251	.419	.419	.083	.419	.503	.419
		000	.042	.008	.008	.167	.419	1.257	.922	3.608	.831	.419	.503	.670	.838
		334	.042	.008	.0008	.008	.084	.419	.671	1.257	.503	.335	.419	.670	.838
		018	.050	.017	.008	.084	.168	.838	.671	1.257	.587	.335	.419	.502	.502
30m		162	.075	.042	.042	.168	.335	1.874	1.676	.838	.587	.335	.410	.419	.419
		136	0	0	0	0	.08	.167	.251	.51	.042	0	0	0	0
		036	0	0	0	0	.08	.167	.21	.13	.042	0	0	0	0
		341	0	0	0	0	0	.042	0	.168	.042	0	0	0	0
		181	.422	.0008	.0008	.001	.008	.251	.167	.419	.167	.167	0	0	0
40m		018	.050	.042	.001	.001	.008	.167	.167	.419	.419	.008	0	0	0
		000	.008	0	0	.001	.008	.251	.251	.587	.084	0	0	0	0
		276	0	0	0	0	0	.08	.001	.13	.008	0	0	0	0
		240	0	0	0	0	.042	.03	.001	.07	.008	0	0	0	0
		122	0	0	0	0	.042	.034	.001	.13	.008	0	0	0	0
		201	.042	.025	.0008	.001	.025	.158	.126	.168	.001	0	0	0	0

θ	Depth	φ	400- 425	425- 450	450- 475	475- 500	500- 525	525- 550	550- 575	575- 600	600- 625	625- 650	650- 675	675- 700	700- 725
40m		070	.025	.017	.0008	.001	.008	.168	.126	.168	.083	.335	.250	.314	.319
		000	.025	.025	.0017	.001	.017	.168	.335	.838	.671	.335	.335	.400	.510
		156	.042	.025	.0017	.0008	.008	.251	.335	.838	.671	.335	.335	.419	.675
		086	0	0	0	0	0	0	0	.008	0	0	0	0	0
50m		000	0	0	0	0	0	0	0	.008	0	0	0	0	0
		151	0	0	0	0	0	0	0	.008	0	0	0	0	0
		037	0	0	0	0	0	0	0	.008	0	0	0	0	0
		000	0	0	0	0	0	0	0	.017	0	0	0	0	0
90° 1m		000	5.53	10.98	16.35	21.79	*	*	*	*	*	*	*	*	*
		066	4.69	8.38	9.64	10.39	17.18	17.10	33.53	*	*	*	*	*	*
		354	5.03	10.06	15.26	20.45	*	*	*	*	*	*	*	*	*
		283	5.11	10.23	15.68	21.79	*	*	*	*	*	*	*	*	*
5m		211	5.03	10.06	15.08	20.28	20.96	20.37	33.53	*	*	*	*	*	*
		160	5.03	9.89	14.92	20.28	*	*	*	*	*	*	*	*	*
		053	4.61	7.96	8.21	20.12	*	*	*	*	*	*	*	*	*
		000	5.36	10.81	16.35	21.96	*	*	*	*	*	*	*	*	*
10m		270	2.01	1.51	2.35	3.52	7.04	10.06	*	*	*	*	27.42	*	*
		213	.59	.75	1.09	1.51	1.34	2.51	5.62	11.74	14.75	6.29	7.54	12.99	36.0
		000	.34	.59	1.09	2.35	4.86	7.46	20.11	*	*	38.98	9.22	12.15	18.44
		276	.08	.08	.08	.34	1.01	1.55	3.35	11.74	3.56	3.35	2.93	3.77	5.45
		221	.34	.34	.42	1.01	1.51	3.35	7.96	39.8	24.3	5.03	3.77	5.87	7.12
		265	.08	.01	.08	.167	.58	.63	.83	6.29	3.56	1.68	1.93	2.93	6.71
		335	.17	.17	.17	.42	1.01	2.51	6.29	18.86	8.80	4.19	3.77	3.77	5.87
		040	.08	.03	.08	.03	.59	1.16	5.45	18.86	8.89	4.19	4.19	5.87	7.12

θ	Depth	φ	400- 425	425- 450	450- 475	475- 500	500- 525	525- 550	550- 575	575- 600	600- 625	625- 650	650- 675	675- 700	700- 725
15m	261	.04	.001	.001	.001	.08	.17	.59	.08	4.61	1.68	.80	.42	.34	0
	306	.03	.01	.01	.01	.01	.08	.21	.75	4.61	2.18	.80	.24	.80	.42
	000	.08	.042	.08	.08	.17	.42	1.09	3.44	11.74	3.56	2.93	2.10	2.51	2.35
	075	.08	.08	.08	.001	.17	.25	.42	1.68	9.22	2.68	2.93	1.26	2.10	2.35
	125	.08	.04	.008	.008	.251	.59	1.09	3.27	10.48	2.68	2.77	1.26	1.68	1.68
20m	094	.042	.042	.008	.008	.168	.335	3.352	3.688	3.269	1.676	1.257	1.676	2.514	2.933
	043	.050	.084	.034	.034	.335	.503	4.191	4.359	1.844	.838	.670	.838	.838	2.096
	315	.084	.034	.001	.001	.042	.168	.839	1.676	4.191	1.006	.67	.838	.754	1.006
	256	.03	.04	0	0	0	.08	.21	.42	2.51	.82	.42	.42	0	0
	000	.08	.08	0	0	0	0	.08	.08	12.99	.42	0	0	0	0
25m	040	.042	.001	.001	.001	.08	.251	.63	1.66	4.61	.75	0	0	0	0
	089	.08	.001	.001	.008	.008	.168	.042	.419	.419	.20	0	0	0	0
	039	.08	*	*	*	*	*	*	*	*	*	*	*	*	*
	321	.08	*	*	*	*	*	*	*	.17	*	*	*	*	*
	179	.067	.017	.001	.001	.001	.008	.168	.042	.419	.419	.251	.167	.251	.838
30m	154	.050	.034	.001	.001	.001	.008	.008	.084	.335	.251	.168	.168	.671	.922
	000	.042	.034	.001	.001	.001	.008	.084	.084	.670	.419	.251	.419	.503	.587
	351	0	0	0	0	0	0	0	0	.17	0	0	0	0	0
	299	0	0	0	0	0	0	0	0	.04	0	0	0	0	0
	000	.042	.034	.0003	.0008	.0008	.0008	.168	.084	.251	.084	.008	0	0	0
40m	031	.042	.034	.0002	.00010	.0001	.008	.084	.042	.251	.008	.008	0	0	0
	235	.042	.034	.0002	.0001	.0001	.008	.042	.0008	.251	.008	0	0	0	0
	306	0	0	0	0	0	.0008	.168	.042	.168	.0008	.008	0	0	0
	083	0	0	0	0	0	.008	.168	.042	.168	.0008	0	0	0	0
	285	0	0	0	0	0	.0008	.084	.0008	0	0	0	0	0	0
40m	142	0	0	0	0	0	.0008	.167	.084	0	0	0	0	0	0
	000	0	0	0	0	0	.0016	.167	.084	0	0	0	0	0	0

θ	Depth	φ	400-		425-		450-		475-		500-		525-		550-		575-		600-		625-		650-		675-		700-		725
			400-	425	425-	450	450-	475	475-	500	500-	525	525-	550	550-	575	575-	600	600-	625	625-	650	650-	675	675-	700	700-		
135°	1m	000	4.28	9.72	14.83	17.60	21.79	23.00	35.53	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
		019	4.36	6.11	5.95	6.20	6.79	8.38	13.41	29.34	44.85	14.67	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	
		325	2.93	2.68	2.43	3.02	2.68	3.58	5.20	9.22	9.22	6.29	12.15	50.29	69.57	*													
		290	3.43	2.18	2.35	3.02	4.86	4.69	5.20	14.67	17.60	11.74	23.89	*	*														
		176	4.53	5.28	3.52	4.36	6.20	6.79	8.38	6.54	8.80	15.93	23.89	0	0														
	5m	115	.502	.42	.67	1.01	1.51	2.35	4.61	9.22	4.19	3.35	5.03	9.47	14.25														
		118	.50	.59	.67	.82	1.51	2.35	5.20	10.05	8.80	5.03	5.87	12.15	2.01														
		000	.50	.67	.59	1.01	1.51	2.35	4.61	10.05	8.80	5.03	5.45	8.13	11.32														
		323	.42	.50	.34	.50	1.17	1.33	3.35	9.22	5.45	3.35	4.36	8.13	18.86														
		248	.34	.42	.25	.50	.82	1.25	2.51	4.61	3.77	2.10	3.35	6.29	10.48														
10m	356	.04	.04	.001	.001	.17	.21	.42	3.77	2.18	.84	.42	.42	.42															
	312	.04	.008	.001	.001	.17	.21	.42	2.51	1.26	.67	.59	.42	.42															
	222	.04	.008	.001	.001	.08	.21	.34	2.18	1.47	.42	.50	0	0															
	255	.04	.008	.001	.001	.08	.21	.42	2.01	.84	.08	.50	0	0															
	000	.04	.008	.001	.001	.17	.25	1.17	4.36	.17	.84	.59	0	0															
15m	040	.04	.008	.001	.001	.04	.13	.01	2.01	.84	.42	.59	0	0															
	222	.04	.008	.001	0	0	0	.08	.13	.08	0	.42	.59	0															
	000	.04	.008	.001	.0001	.0001	.08	.17	.84	.84	.0001	.50	.42	.42															
	022	.008	.008	.001	0	0	.03	.08	.42	.42	0	.50	.42	.42															
	124	.001	.001	.001	0	0	.08	.17	.63	.68	0	.50	.42	.42															
15m	355	.034	.001	.0008	.0008	.008	.419	.335	.335	.419	.084	.251	.084	.084															
	246	.0008	.0008	.0008	.0008	.0008	.084	.168	.838	.419	.251	.008	.838	.838															

Depth	φ	400-425-		450-475-		500-		525-		550-		575-		600-		625-		650-		675-		700-	
		400	425	450	475	500	525	550	575	600	625	650	675	700	725	750	775	800	825	850	875	900	925
20m	339	0	0	0	0	0	0	0	0	.08	0	0	0	0	0	0	0	0	0	0	0	0	0
	000	0	0	0	0	0	0	0.1	2.0	.28	0.1	0	0	0	0	0	0	0	0	0	0	0	0
	103	0	0	0	0	0.1	1.4	4.5	.08	.08	.08	0	0	.08	0	0	0	0	0	0	0	0	0
	143	.01	0	0	0	0	0	0	0	.08	0	0	0	.08	0	0	0	0	0	0	0	0	0
	184	.017	.0008	0	0	0	.084	.084	.419	.419	.419	.017	0	.017	0	0	0	0	0	0	0	0	0
25m	201	0	0	0	0	0	.059	.084	.419	.419	.001	.008	0	0	0	0	0	0	0	0	0	0	0
	208	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	182	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	343	0	0	0	0	0	.084	.0008	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	000	0	0	0	0	0	.084	.0008	.0001	.0001	.042	0	0	.042	0	0	0	0	0	0	0	0	0
	090	0	0	0	0	0	.067	.042	.419	.419	.084	0	0	.084	0	0	0	0	0	0	0	0	0
	110	0	0	0	0	0	.067	.042	.419	.419	.084	0	0	.084	0	0	0	0	0	0	0	0	0

θ	Depth	φ	400-	425-	450-	475-	500-	525-	550-	575-	600-	625-	650-	675-	700-	725-
			425	450	475	500	525	550	600	625	650	675	700	725		
166°	1m	000	4.95	9.47	12.57	9.72	17.6	20.12	33.53	*	*	31.43	30.60	*	*	
		082	1.84	1.68	1.93	2.68	2.68	3.98	5.87	10.06	9.22	7.96	5.51	6.28	*	
		150	*	5.196	5.700	6.538	6.873	7.711	15.088	39.396	45.264	16.764	*	*	*	
	5m	000	.34	.34	.25	.50	.92	1.26	2.51	6.54	3.10	2.77	3.77	6.29	10.06	
		205	.34	.50	.34	.80	.92	1.26	2.51	6.29	3.77	4.19	3.35	6.29	11.32	
	10m	000	.04	.01	.001	.001	.08	.13	.42	2.01	.84	.25	.59	.42	.42	
		270	.04	.01	.001	.001	.08	.13	.42	.84	.84	.08	.42	0	.08	
		055	.03	.01	.001	.001	.08	.13	.42	.84	.50	.17	.50	0	.42	
	15m	120	.04	.001	.001	.001	.001	.001	.08	.17	.42	.001	.34	.001	.001	
		000	.03	.01	.001	.001	.001	.001	.08	.21	.50	.08	.42	.001	.001	
	20m	000	0	0	0	0	0	0	.0011	.112	.001	0	0	0	0	
	25m	000	0	0	0	.0008	0	.067	.0008	0	.042	0	0	0	0	

* Values exceed limitations of standard lamp

BIBLIOGRAPHY

1. Austin, R. W. and T. J. Petzold 1968. An Underwater Transmissometer for Ocean Survey Work. Scripps Institution of Oceanography Reference No. 68-9.
2. Austin, R. W. and R. W. Loudermilk 1968. An Oceanographic Illuminator for Light Penetration and Reflection Studies. Scripps Institution of Oceanography Reference No. 68-11.
3. Bassett, C. H. and H. C. Furminger 1965. An Investigation of Light Scattering in Monterey Bay. M.S. Thesis, Naval Postgraduate School.
4. Burt, W. V. 1955. Interpretation of Spectrophotometer Readings on Chesapeake Bay Water. Journal of Marine Research, Vol. 14, pp. 33-47.
5. Busby, R. F. 1967. Undersea Penetration by Ambient Light and Visibility. Science, Vol. 158, No. 3805, pp. 1178-80.
6. Clarke, G. L. and E. J. Denton 1962. Light and Animal Life, The Sea, Vol. I, Ed. M. N. Hill. New York: Interscience.
7. Duntley, S. Q. 1963. Light in the Sea. Journal of the Optical Society of America, Vol. 53, No. 2, pp. 214-233.
8. Ivanoff, A. and T. H. Waterman 1958. Factors, Mainly Depth and Wavelength, Affecting the Degree of Underwater Light Polarization. Journal of Marine Research, Vol. 10, No. 3, pp. 283-307.
9. Ivanoff, A., N. G. Jerlov and T. H. Waterman 1961. A Comparative Study of Irradiance, Beam Transmittance and Scattering in the Sea Near Bermuda. Limnology and Oceanography, Vol. 8, No. 2, pp. 129-148.
10. Jerlov, N. G. 1953. Influence of Suspended and Dissolved Matter on the Transparency of Sea Water. Tellus, Vol. 5, No. 1, pp. 59-65.
11. Jerlov, N. G. and J. Piccard 1959. Bathyscaph Measurements of Daylight Penetration in the Mediterranean. Deep-Sea Research, Vol. 5, No. 3, pp. 201-204.
12. Jerlov, N. G. and M. Fukuda 1960. Radiance Distribution in the Upper Layers of the Sea. Tellus, Vol. 12, No. 3, pp. 348-355.

13. Jerlov, N.G. 1964. Optical Classification of Ocean Water. In: Physical Aspects of Light in the Sea. Honolulu: Univ. Hawaii Press, pp. 45-49.
14. Jerlov, N.G. 1968. Optical Oceanography. Amsterdam: Elsevier Publishing Company.
15. Karabashev, G. S. 1966. A Photometer for Measuring Spectral Function of Irradiance Attenuation in the Sea. Oceanology, Vol. 6, No. 5, pp. 722-726.
16. Karelin, A. K. and V. N. Pelevin 1970. The FMPO-64 Marine Underwater Irradiance Meter and Its Application in Hydro-Optical Studies. Oceanology, Vol. 10, No. 2, pp. 282-285.
17. Kodak Wratten Filters for Scientific and Technical Use. 1965. 22nd Ed., Eastman Kodak Company.
18. Lawrence, L.G. 1967. Electronics in Oceanography. Indianapolis: Howard W. Sams & Co., Inc., pp. 174-180.
19. Neumann, G. and W. J. Pierson, Jr., 1966. Principles of Physical Oceanography. Englewood Cliffs: Prentice Hall Inc.
20. Preisendorfer, R. W. 1959. Theoretical Proof of the Existence of Characteristic Diffuse Light in Natural Waters. Journal of Marine Research, vol. 18, pp. 1-9.
21. Sasaki, T., et al. 1955a. Optical Properties of the Water in the Kuroshio Current. Records of Oceanographic Works in Japan, Vol. 2, No. 2, pp. 1-8.
22. Sasaki, T., et al. 1955b. Measurements of the Angular Distribution of Submarine Daylight. Journal of the Scientific Institute, No. 1,387, Vol. 49, pp. 103-106, Tokyo, Japan.
23. Sasaki, T., et al. 1957. Measurements of the Angular Distribution of Daylight in the Sea. Records of Oceanographic Works in Japan (Special Number, March 1957), pp. 42-45.
24. Sasaki, T., et al. 1960a. Measurements of Perpendicular and Horizontal Angular Distribution of Submarine Daylight by Means of New Remote Control Instrument. Records of Oceanographic Works in Japan (Special No. 4), pp. 197-205.
25. Sasaki, T., et al. 1960b. Angular Distribution of Scattered Light in Deep Sea Water. Records of Oceanographic Works in Japan, Vol. 5, No. 2, pp. 1-10.
26. Sasaki, T., et al. 1962. On the Instrument for Measuring Angular Distribution of Underwater Radiance. Bulletin of the Japanese Society of Scientific Fisheries, Vol. 28, No. 5, pp. 489-496.

27. Sasaki, T., G. Oshiba and M. Kishino 1966. A 4 π Underwater Irradiance Meter. Journal of Oceanographic Society of Japan, Vol. 22, No. 4, pp. 1-6.
28. Sasaki, T., et al. 1968. Optical Properties of the Water in Adjacent Regions of the Kuroshio. Journal of Oceanographic Society of Japan, Vol. 24, No. 2, pp. 45-50.
29. Smith, R. C. and J. E. Tyler 1967. Optical Properties of Clear Natural Water. Journal of the Optical Society of America, Vol. 57, No. 5, pp. 589-595.
30. Tyler, J. E. and R. W. Preisendorfer 1962. Transmission of Energy Within the Sea, The Sea, Vol I., Ed. M. N. Hill, New York: Interscience.
31. Tyler, J. E. and R. C. Smith 1966. Submersible Spectroradiometer. Journal of the Optical Society of America, Vol. 56, No. 10, pp. 1390-1396.
32. Tyler, J. E. and R. C. Smith 1967. Spectroradiometric Characteristics of Natural Light Underwater. Journal of the Optical Society of America, Vol. 57, No. 5, pp. 595-601.
33. Tyler, J. E. and R. C. Smith 1970. Measurements of Spectral Irradiance Underwater. New York: Gordon and Breach, Science Publishers.
34. Whitney L. V. 1961. General Law of Diminution of Light Intensity in Natural Waters and % of Diffuse Light at Different Depths. Journal of Optical Society of America, Vol. 31, No. 12, pp. 714-722.
35. Williams, Jerome 1970. Optical Properties of the Sea. Annapolis: United States Naval Institute.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Documentation Center Cameron Station Alexandria, Virginia 22314	2
2. Library, Code 0212 Naval Postgraduate School Monterey, California 93940	2
3. Assistant Professor Stevens P. Tucker, Code 58Tc Department of Oceanography Naval Postgraduate School Monterey, California 93940	6
4. LT Raymond T. Michelini, USN COMCRUDESFLOT TWELVE FPO New York 09501	3
5. Department of Oceanography Naval Postgraduate School Monterey, California 93940	3
6. Commanding Officer and Director Naval Undersea Research & Development Center Attn: Code 2230 San Diego, California 92152	1
7. Director, Naval Research Laboratory Attn: Tech. Services Info. Officer Washington, D. C. 20390	1
8. Office of Naval Research Department of the Navy Washington, D. C. 20360	1
9. Oceanographer of the Navy The Madison Building 732 N. Washington Street Alexandria, Virginia 22314	1
10. Library USCG Oceanographic Unit Bldg. 159E, Navy Yard Annex Washington, D. C. 20390	1

11. Prof. Kendall L. Carder 1
Marine Science Institute
University of South Florida
830 First Street South
St. Petersburg, Florida 33701
12. Naval Oceanographic Office 1
Attn: Library
Washington, D. C. 20390
13. Director, Maury Center of Ocean Sciences 1
Naval Research Laboratory
Washington, D. C. 20390
14. Mr. Roswell W. Austin 1
Visibility Laboratory
Scripps Institution of Oceanography
La Jolla, California 92037
15. Dr. Wayne V. Burt 1
Department of Oceanography
Oregon State University
Corvallis, Oregon 97331
16. Dr. Peyton Cunningham 6
Department of Physics
Naval Postgraduate School
Monterey, California 93940
17. Dr. Siebert Q. Duntley 1
Visibility Laboratory
Scripps Institution of Oceanography
La Jolla, California 92037
18. Mr. George Eck 1
Naval Air Development Center
Johnsville, Warminster, Pennsylvania 18974
19. Mr. Gary Gilbert 1
Stanford Research Institute
Menlo Park, California 94025
20. Dr. R. C. Honey 1
Stanford Research Institute
Menlo Park, California 94025

21. Mr. Kenneth V. Mackenzie 1
Ocean Sciences Department, Code D503
Naval Undersea Research & Development Center
San Diego Division
San Diego, California 92152
22. Dr. Robert E. Morrison 1
AE1
Office of Environmental Systems
N.O.A.A.
6010 Executive Blvd.
Rockville, Maryland 20852
23. Mr. Larry Ott 2
Naval Air Development Center
Johnsville, Warminster, Pennsylvania 18974
24. Mr. Robert Owen 1
National Marine Fisheries Service
P.O. Box 271, La Jolla, California 92037
25. Mr. James Reese 1
Ocean Sciences Department Code D503
Naval Undersea Research & Development Center
San Diego Division
San Diego, California 92152
26. Mr. John E. Tyler 1
Visibility Laboratory
Scripps Institution of Oceanography
La Jolla, California 92037
27. Dr. Hasong Pak 1
Department of Oceanography
Oregon State University
Corvallis, Oregon 97331
28. Mr. John Arvesen 1
Mail Stop 234-1
Ames Research Center
Moffett Field, California 94035
29. Mr. Alan Baldridge, Librarian 1
Hopkins Marine Station
Pacific Grove, California 93950

30. Mr. Ted Petzold 1
Visibility Laboratory
Scripps Institution of Oceanography
La Jolla, California 92037
31. Director 1
Moss Landing Marine Laboratories
Moss Landing, California 95039
32. Mrs. Elsie F. DuPre 1
Oceanography Branch, Optical Sciences Division
Naval Research Laboratory
Washington, D. C. 20390
33. Mr. W. J. Stachnik 1
Optical Systems
U. S. Navy Underwater Sound Laboratory
Fort Trumbull
New London, Connecticut 06320
34. Mr. Raymond N. Vranicar 2
Code AIR-370D
Naval Air Systems Command
Washington, D. C. 20360
35. Mr. Irvin H. Gatzke 2
Code AIR-370
Naval Air Systems Command
Washington, D. C. 20360
36. Mr. Joseph R. Gerber 1
9 Colonial Drive
Allendale, New Jersey 07401
37. Dr. Sydney H. Kalmbach 1
Department of Physics
Naval Postgraduate School
Monterey, California 93940
38. Dr. Ned A. Ostenso 1
Office of Naval Research
Code 480D
Arlington, Virginia 22217

39. DZ.Y2B 1
Yavuz Ergengil
Muhtesip Iskender Mah.
Akseki Cad. No. 24
Fatih-Istanbul, Turkey
40. Department of Oceanography 1
United States Naval Academy
Annapolis, Maryland 21402

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author)

Naval Postgraduate School
Monterey, California 93940

2a. REPORT SECURITY CLASSIFICATION

Unclassified

2b. GROUP

3. REPORT TITLE

Spectral Radiance Measurements in Monterey Bay

4. DESCRIPTIVE NOTES (Type of report and, inclusive dates)

Master's Thesis; September 1971

5. AUTHOR(S) (First name, middle initial, last name)

Raymond Theodore Michelini

6. REPORT DATE

September 1971

7a. TOTAL NO. OF PAGES

86

7b. NO. OF REFS

35

8a. CONTRACT OR GRANT NO.

b. PROJECT NO.

c.

d.

9a. ORIGINATOR'S REPORT NUMBER(S)

9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report)

10. DISTRIBUTION STATEMENT

Approved for public release; distribution unlimited.

11. SUPPLEMENTARY NOTES

12. SPONSORING MILITARY ACTIVITY

Naval Postgraduate School
Monterey, California 93940

13. ABSTRACT

An underwater spectral radiance meter having a rotating spectral wedge filter and capable of operating to depths of 300 meters was designed and constructed. It was used to obtain measurements of spectral radiance to a depth of 60 meters at two stations in southern Monterey Bay, California, on an overcast day during July 1971. Variations of the spectral radiance distribution with depth were plotted for vertical angles of 0, 45, 90, 135 and 166 degrees at an azimuth angle of zero degrees with respect to the sun.

The results of the measurements are reasonable in all cases and indicate that the spectral wedge filter provides a practical means of determining spectral radiance distributions.

KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Radiance Optical Oceanography Spectral Radiance Hydrological Optics Optical Properties of Sea Water Light Penetration of Sea Water, Monterey Bay, Calif. Light in the Sea						

Thesis
M57534
c.2

Michelini

Spectral radiance
measurments in Mon-
terey Bay.

131296

Thesis
M57534
c.2

Michelini

Spectral radiance
measurments in Mon-
terey Bay.

131296

thesM57534

Spectral radiance measurements in Monter



3 2768 001 88313 5

DUDLEY KNOX LIBRARY